

FY21 SMALL AREA STUDY I-81 EXIT 235 AND ROUTE 256

## FY 2021 SMALL AREA STUDY

## I-81 Exit 235 and Route 256

July 2022

Prepared for:

Staunton Augusta Waynesboro Metropolitan Planning Organization
Prepared by:
Michael Baker
INTERNATIONAL

## TABLE OF CONTENTS

1. Introduction.. .....  1
1.1 Study Area and Stakeholders ..... 1
2. Existing Conditions ..... $\ldots . . .2$
2.1 Traffic Conditions and Data .....  2
3. Future Traffic Conditions .....  .8
3.1 Future Growth .....  8
3.2 Funded Traffic Improvements .....  8
3.3 Future No Improvement Traffic Operations .....  8
4. Alternatives Analysis .....  11
4.1 Intersection of US Route 11 and Route 256 .....  11
4.2 I-81 and Route 256 interchange ..... 13
5. Conceptual Level Construction Costs and Impacts .....  15
5.1 Intersection of US Route 11 and Route 256 .....  15
$5.2 \mathrm{I}-81$ and Route 256 interchange .....  15
6. Public Involvement Results .....  16
6.1 Intersection of US Route 11 and Route 256 .....  16
6.26 .2 1-81 and Route 256 interchange .....  16
7. Conclusions and Recommendations .....  17
APPENDICES
8. Appendix A: Route 256 Area Plan - Base Year Volumes and Future Growth Rates ..... A-1
9. Appendix B: Synchro Report - Existing Conditions ..... A-7
10. Appendix C: Synchro Report - Future No-Build Conditions ..... A-24
11. Appendix D: Synchro Report - Future Build Conditions ..... A-4
12. Appendix E: SIDRA Report - Future Build Conditions ..... A-54
LIST OF TABLES
Table 1. Synchro Analysis: Intersection of US Route 11 and Route 256 .....  2
Table 2. Synchro Analysis: Intersection of Southbound I-81 Ramp and Route 256 .....  5
Table 3. Synchro Analysis: Intersection of Northbound I-81 Ramp and Route 256 .....  .6
Table 4. Synchro Analysis: Triangle Drive and Route 256 .....  7
Table 5. US 11: 2045 Operational Results for Alternatives. .....  12
Table 7. I-81 Interchange: Operational Results for Alternatives (Northbound) .....  14
Table 6. I-81 Interchange: Operational Results for Alternatives (Southbound) .....  14
Table 8. US 11: Construction Cost Ranges and Right-of-Way Impacts .....  15
Table 9. I-81 Interchange: Construction Cost Ranges and Right-of-Way Impacts. .....  15
LIST OF FIGURES
Figure 1. Study Area .....  1
Figure 2. Recommended Base Year Volumes .....  3
Figure 3. Crashes by Type .....  4
Figure 4. Crashes by Severity .....  4
Figure 5. Intersection Level of Service Summary .....  5
Figure 6. Crashes at US Route 11 .....  5
Figure 7. Crashes at Intersection of Southbound I-81 Ramp and Route 256 .....  6
Figure 8. Crashes at I-81 Northbound Ramp .....  6
Figure 9. Crashes at the Intersection of Triangle Drive and Route 256 .....  7
Figure 10. Funded Traffic Improvements .....  8
Figure 11. 2045 Future Volumes .....  9
Figure 12. Future No Improvement .....  10
Figure 13. US 11: Minimally Managed Improvements .....  11
Figure 14. US 11:Single-Lane Roundabout .....  11
Figure 15. I-81 Interchange: Single-Lane Teardrop Roundabout .....  13
Figure 16. I-81 Interchange: Three-Lane Bridge .....  13
Figure 17. US 11: Metroquest Summary .....  16
Figure 18. I-81 Interchange: Metroquest Summary .....  16

## 1. INTRODUCTION

The Weyers Cave area has experienced an increase in traffic levels due to industrial, institutional, commercial, and residential development in the vicinity of the I-81 interchange at Route 256 (Exit 235). Exit 235 serves several regional generators including Blue Ridge Community College and the Shenandoah Valley Regional Airport. With Weyers Cave's status as a Designated Growth Area, future traffic conditions are anticipated to present several challenges to both motorized and non-motorized travelers. The Exit 235 Small Area Study seeks to identify and evaluate solutions to address periodic congestion at the Exit 235 Interchange, anticipate long-term corridor needs and accommodate future growth.

### 1.1 Study Area and Stakeholders

The study area extends along Weyers Cave Road (VA 256) from Lee Highway (US 11) in the west to Triangle Drive in the east as shown in Figure 1. The study area is approximately four-tenths ( 0.4 ) of a mile in length and includes the following intersections

Route 256 and US Route 11

- Route 256 and Southbound I-81 Ramp
- Route 256 and Northbound I-81 Ramp
- Route 256 and Triangle Drive

The study included a diverse stakeholder group that represents local, regional, and state goals for the Weyers Cave area. These members are:

- Staunton Augusta Waynesboro Metropolitan Planning Organization (SAWMPO)
- Central Shenandoah Planning District Commission (CSPDC)
- Blue Ridge Community College (BRCC)
- Shenandoah Valley Regional Airport (SVRA)
- Augusta County
- Virginia Department of Transportation (VDOT)
- Michael Baker International



## 2. EXISTING CONDITIONS

### 2.1 Traffic Conditions and Data

The study area existing conditions are based on 2021 traffic data and field visits. The study team performed a field visit on May 5, 2021 to help verify operational and safety concerns. Data collection included obtaining turn movement counts on April 13, 2021 and 2015-2019 crash data from VDOT. It should be noted that the traffic counts were calibrated due to COVID-19 impacts on travel patterns. The base year volumes are shown in Figure 2. The detailed process to develop these volumes can be found in Appendix A.

Crash data analyses included a review of time of day, weather conditions, crash severity, and crash type. Figures 3 and 4 show both the crash types and crash severity along the study area.

Finally, traffic operations were analyzed in accordance with the Traffic Operations and Safety Analysis Manual 2.0 (TOSAM). The study team updated the 2017 VDOT Synchro model with the base year volumes for peak hours between 7:15 AM to 8:15 AM and 4:30 PM to 5:30 PM. Measures of effectiveness for intersections include Highway Capacity Manual (HCM) control delay (seconds/vehicle) and Synchro 95th percentile queue length. Control delay is delay brought about by the presence of a traffic control device, including delay associated with vehicles slowing in advance of an intersection, the time spent stopped on an intersection approach, the time spent as vehicles move up in the queue, and the time needed for vehicles to accelerate to their desired speed. Whereas the queue length is the distance between the upstream and downstream ends of the queue. Figure 5 summarizes the intersection level of service (LOS), which is a graded measure of the operating conditions of a roadway.

### 2.1.1 Intersection of US Route 11 and Route 256

The intersection of US Route 11 and Route 256 is an existing signalized intersection controlling five approaches, one on Route 256 in the westbound direction, one on Ridgetop Drive (a private roadway) in the eastbound direction, two on US Route 11, and one from an inactive gas station (as of June 2021) in the southwest corner. The southbound US Route 11 left-turn is protected-permitted with a five-section traffic signal face, and the northbound left-turn is permissive. There is also a static flashing beacon for northbound US Route 11 drivers approaching the traffic signal. Other observations and comments from stakeholders include:

- Wide intersection due to traffic signal placement
- Queuing from I-81 southbound ramp nearing the US Route 11 and Route 256 intersection
- Driver confusion from left-turning vehicles making a left from southbound US Route 11 onto Route 256
- Sight distance is limited due to the vertical curve when approaching the signal on northbound US Route 11 This obstructs the traffic signal indication, however, the flashing beacon is placed in advance notifying roadway users a traffic signal is ahead
- This issue also affects drivers ability to see approaching vehicles when making a permissive left-turn from southbound US Route 11
- Rutting in the northwest corner from vehicles making a right onto northbound US Route 11 from Route 256 Synchro analysis results can be found in Table 1.

Table 1. Synchro Analysis: Intersection of US Route 11 and Route 256

| Direction | Lane Group | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (Sec/ veh) | LOS | $\text { Length ( } \mathrm{ft} \text { ) }$ | Delay (Sec/ veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length }(\mathrm{ft}) \end{gathered}$ |
| Ridgetop DriveEastbound | Left | 21.8 | c | - | 26.0 | c | - |
|  | Through | 21.8 | c | 20 | 26.0 | c | 9 |
|  | Right | 21.8 | c | - | 26.0 | C | - |
| Route 256 Westbound | Left | 48.6 | D | 483 | 37.7 | D | 130 |
|  | Through | 48.6 | D | 483 | 37.7 | D | 130 |
|  | Right | 22.4 | C | 0 | 26.8 | C | 12 |
| US 11 Northbound | Left | 34.2 | C | 16 | 26.3 | c | 20 |
|  | Through | 43.4 | D | 155 | 31.6 | c | 136 |
|  | Right | 34.9 | c | 0 | 27.7 | c | 42 |
| US 11 Southbound | Left | 31.8 | c | 155 | 17.9 | B | 176 |
|  | Through | 24.4 | c | 136 | 15.3 | B | 149 |
|  | Right | 24.4 | c | 136 | 15.3 | B | 149 |
| Gas Station | Left | 47.1 | D | 0 | 38.1 | D | 0 |
|  | Through | 47.1 | D | - | 38.1 | D | - |
|  | Right | 47.1 | D | 0 | 38.1 | D | 0 |
| Overall |  | 37 | D | - | 25.4 | c | - |

Figure 2. Recommended Base Year Volumes


Figure 3. Crashes by Type


Figure 4. Crashes by Severity



As shown in Table 1, The intersection experiences more delay in the AM peak period, than the PM peak period. This is a result of a higher left-turn volume movement from Route 256 onto southbound US Route 11, where vehicles experience 48.6 seconds/vehicle of delay. In the PM peak period, traffic delay is less than the AM, however the westbound and northbound movements still experience delay of about 30 seconds/vehicle.

Crash summary results can be found in figure 6 .
The most frequent crash type at this intersection is an angle crash. These crashes typically involved either northbound left-turns from US Route 11 onto Ridgetop Drive with the southbound US Route 11 through movement or vehicles entering/exiting the BP gas station driveway. As mentioned previously, the intersection is wide and the northbound stop bar significantly set back from where most movements occur. In addition, the combination of turning distance lengths and the permissive green can contribute to driver right-of-way confusion. Finally, the BP gas station driveways do not meet access management standards which, increases the risk of these types of crashes.

Figure 6. Crashes at US Route 11

2.1.2 Intersection of Southbound I-81 Ramp and Route 256

The intersection of the southbound I-81 Ramp and Route 256 is an existing signalized intersection controlling vehicles entering and exiting between Route 256 and I-81. No turn lanes exist on any approach, although passenger vehicles were observed using the additional pavement width on the southbound off-ramp to make a right onto Route 256. Other observations and comments from stakeholders include:

- Left-turns have a leading signal phase to enter the I-81 southbound ramp
- Queuing was observed between the two ramp signals, although queues did clear each cycle
- Rutting is observed between the shoulder and pavement on the southbound I-81 ramp
- Stakeholders mention that operations do get worse during incidents and James Madison University sporting events Synchro analysis results can be found in Table 2.

Table 2. Synchro Analysis: Intersection of Southbound I-81 Ramp and Route 256

| Direction | Lane Group | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (Sec) veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length }(\mathrm{ft}) \\ \hline \end{gathered}$ | Delay (Sec/ veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length (ft) } \end{gathered}$ |
| Route 256 Eastbound | Through | 16.8 | B | 302 | 41.0 | D | 471 |
|  | Right | 16.8 | B | 302 | 41.0 | D | 471 |
| Route 256 Westbound | Left | 16.6 | B | 359 | 15.3 | B | 185 |
|  | Through | 16.6 | B | 359 | 15.3 | B | 185 |
| $\begin{gathered} \text { I-81 } \\ \text { Southbound } \end{gathered}$ | Left | 51.7 | D | 222 | 41.0 | D | 255 |
|  | Through | 51.7 | D | 222 | 41.0 | D | 255 |
|  | Right | 51.7 | D | 222 | 41.0 | D | 255 |
| Overall |  | 24.9 | C | - | 33.6 | c | - |

As a result of no turn lanes and the high left and right-turning volumes, the intersection experiences delays and queue that impact through traveling vehicles today. The AM peak period experiences an intersection delay of 24.9 seconds/ vehicle with relatively minimal issues on most approaches. However during the PM peak period, the intersection experiences more delay on all approaches. The intersection delay is 33.6 seconds/vehicle and consistent queuing on all approaches, the worst being the eastbound approach at 471 feet.

Crash summary results can be found in figure 7.

Figure 7. Crashes at Intersection of Southbound I-81 Ramp and Route 256


Approximately half of the rear-end crashes are occurring westbound on Route 256. Rear-end crashes also occurred on the southbound I-81 ramp, and eastbound on Route 256. The crashes at this intersection can be attributed to the lack of turn lanes, which could provide refuge for turning vehicles and improve operations.
2.1.3 Intersection of Northbound I-81 Ramp and Route 256

The intersection of the northbound I-81 Ramp and Route 256 is an existing signalized intersection controlling vehicles entering and exiting between Route 256 and $\mathrm{I}-81$. None of the four approaches has a turn lane. Other observations and comments from stakeholders include:

- Left-turns have a leading signal phase to enter the I-81 northbound ramp
- Queuing was observed between the two ramp signals, although not as bad as the southbound I-81 ramp
- Queuing was also observed between the signal and Triangle Drive
- Stakeholders mention that operations do get worse during incidents and James Madison University events, especially with vehicles attempting to make a left from I-81 northbound to Route 256 westbound
Synchro analysis results can be found in Table 3.

Table 3. Synchro Analysis: Intersection of Northbound I-81 Ramp and Route 256

| Direction | Lane Group | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (Sec/ veh) | LOS | Queue Length $(\mathrm{ft})$ | Delay (Sec/ veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length ( } \mathrm{ft} \text { ) } \\ \hline \end{gathered}$ |
| Route 256 Eastbound | Left | 11.6 | B | 159 | 6.7 | A | 108 |
|  | Through | 11.6 | B | 159 | 6.7 | A | 108 |
| Route 256 Westbound | Through | 24.5 | C | 536 | 22.8 | C | 347 |
|  | Right | 24.5 | C | 536 | 22.8 | c | 347 |
| 1-81NorthboundRamp | Left | 54.2 | D | 257 | 33.4 | c | 132 |
|  | Through | 54.2 | D | 257 | 33.4 | c | 132 |
|  | Right | 54.2 | D | 257 | 33.4 | C | 132 |
| Overall |  | 27.5 | C | - | 17.3 | B | - |

As a result of no turn lanes and the high left and right-turning volumes, the intersection does experience delays and queues that impact through traveling vehicles. The AM peak period experiences an intersection delay of 27.5 seconds/ vehicle with relatively minimal issues on most approaches. During the PM peak the intersection experiences 17.3 seconds/vehicle and consistent queuing on all approaches. In both instances, the westbound Route 256 movement experiences similar delay and queues. The westbound Route 256 AM approach delay is 24.5 seconds/vehicle and the PM approach delay is 22.8 seconds/vehicle.

Crash summary results can be found in Figure 8.
Most rear end crashes either occurred in the eastbound or westbound directions on Route 256. These crashes can be attributed to the lack of turn lanes at the intersection. Turn lanes could provide refuge for turning vehicles and improve operations.

2.1.4 Intersection of Triangle Drive and Route 256

The intersection of Triangle and Route 256 is an unsignalized intersection with minor street stop-control. The intersection serves a gas station and an industrial area to the south. No turn lanes exist on any approach. Other observations and comments from stakeholders include:

- Rutting was observed on the right-side approach of the intersection
- Traffic signage (as of June 2021) looks to have been hit
- Sight distance is adequate in both directions
- Queue's had been observed near Triangle Drive on Route 256 as result of the northbound I-81 ramp traffic signal

Synchro analysis results can be found in Table 4.

Table 4. Synchro Analysis: Triangle Drive and Route 256

| Direction | Lane Group | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (Sec/ veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length ( } \mathrm{ft} \text { ) } \end{gathered}$ | Delay (Sec/ veh) | LOS | $\begin{gathered} \text { Queue } \\ \text { Length }(\mathrm{ft}) \\ \hline \end{gathered}$ |
| Route 256 <br> Eastbound | Through | 0.0 | A | 0 | 0.0 | A | 0 |
|  | Right | 0.0 | A | 0 | 0.0 | A | 0 |
| Route 256 Westbound | Left | 0.7 | A | 2 | 0.9 | A | 2 |
|  | Through | 0.7 | A | 2 | 0.9 | A | 2 |
| Triangle Dr. Northbound | Left | 29.0 | D | 32 | 41.2 | E | 82 |
|  | Right | 29.0 | D | 32 | 41.2 | E | 82 |
| Overall |  | 2.1 | A | - | 4.5 | A | - |

The intersection of Triangle Drive and Route 256 is an existing unsignalized intersection with minor stop-control The intersection serves a gas station and an industrial area to the south. No turn lanes exist on any approach. Othe observations and comments from stakeholders include:

Crash summary results can be found in figure 9 .
This intersection was not observed to have any significant crash issues. The two angle crashes involved left-turning vehicles on Route 256 onto Triangle Drive with through-bound Route 256 vehicles. The one rear-end was a result of a left-turning Route 256 vehicle turning onto Triangle Drive being struck by a Route 256 through-bound vehicle.

Figure 9. Crashes at the Intersection of Triangle Drive and Route 256


## 3. Future Traffic Conditions

### 3.1 Future Growth

The stakeholder group agreed on a 2045 forecast year to evaluate future operations of the study intersections. The study team then developed growth rates in accordance with IIM-TMPD-7.0 Traffic Forecasting. The growth rates were based on the Staunton Augusta Waynesboro MPO Travel Demand Modal, historical volumes, funded developments, and planned expansions at SVRA and BRCC. Appendix A documents development of the growth rates. VDOT TMPD and the stakeholder group approved the growth rates on June 10, 2021. The 2045 traffic volumes can be found in Figure 11 and are based on the following assumptions:

- $1 \%$ background linear growth rate applied to Route 256
- Apply the same methodology for the I-81 ramp Volumes as the March 2021 Memo
- $2.00 \%$ linear growth rate be applied to the daily ramp volume estimate by dividing the 2017, 12 -hour turning movement counts by 0.75
- The additional volume will be carried back towards the east on Route 256 to account for the higher growth associated with the airport and planned improvements to the east
- $1 \%$ linear growth rate applied to US 11
- Zero or no growth for the northbound approach of Triangle Drive
- Site Traffic ITE Calculation for the funded Park and Ride Lot entrance at Triangle Drive using ITE Trip Generation Code 090 - Park and Ride Lot with Bus or Light Rail
- Site Traffic ITE Calculation for the Landings Drive Weyers Caver Apartment Complex using the highest of the two ITE Trip Generation Codes 221 - Multifamily Housing (Mid-Rise) or 231 - Mid Rise with 1st Floor Commercial


### 3.2 Funded Traffic Improvements

There are multiple funded improvements on the Route 256 corridor that are expected to be completed before the analysis year. These improvements include

- Intersection of Southbound I-81 Ramp and Route 256: eastbound Route 256 right-turn lane
- Intersection of Northbound I-81 Ramp and Route 256: westbound Route 256 right-turn lane
- Park N' Ride lot located on north side of Route 256 between the northbound I-81 ramp and Triangle Drive
- Shared use path on south side of Route 256 between the northbound I-81 ramp and the gas station
- Westbound Route 256 left-turn lane at Triangle Drive

Figure 10 summarizes all improvements in one concept.

### 3.3 Future No Improvement Traffic Operations

The Synchro models were updated with 2045 volumes, the funded improvements, and optimized signal timings. Detailed results of the no improvements can be found in Section 4. Figure 12 summarizes the future No Improvement conditions on Route 256.

In general, operational delay worsens for all intersections by 2045. The AM overall intersection delay increases from 37.0 seconds/vehicle to 47.4 seconds/vehicle. At both ramps the right-turn lanes help the approaches for those directions, however, the overall ramp operations will get worse and be over capacity with the possibility of queues backing-up into upstream intersections impacting those operations.

Figure 10. Funded Traffic Improvements


Saw/mpo july 2022

Figure 11. 2045 Future Volumes


Figure 12. Future No Improvement


## 4. Alternatives Analysis

The study team and stakeholders determined to move forward with an alternatives analysis on all intersections but Triangle Drive and Route 256. However, this intersection should be monitored once the funded improvements are constructed and if additional development occurs on the northside of Route 256. The study team's goal was to develop multiple alternatives that would address current and future needs. Each alternative was focused on providing innovative ways to enhance safety and improve operations.
The study team evaluated multiple options that addressed context, operations, and safety when developing alternatives for each intersection. A preliminary analysis was performed using the VDOT Junction Screening Tool (VJuST) to evaluate Volume-to-Capacity (V/C) ratios (when applicable) and conflict points to help screen initial ideas. The stakeholder group review all initial concepts to determine what would advance to the detailed alternatives analysis. The detailed analyses were reviewed in SIDRA and Synchro. The analyses also evaluated the crash modification factor (CMF) for each alternative. CMFs are research developed percentages which demonstrates the anticipated crash reduction of an improvement. The CMF provided in this report are from the VDOT SMART SCALE preferred CMF list. These alternatives were advanced for further review by stakeholders and the public.

### 4.1 Intersection of US Route 11 and Route 256

Each proposed recommendation at US Route 11 and Route 256 requires the reconstruction of Ridgetop Drive, which is presented in each alternative figure. The reconstruction of Ridgetop Drive does assume to be built to VDOT roadway design standards.
4.1.1 Minimally managed improvements

This alternative removes the traffic signal phase for the southwest gas station. The access to the southwest gas station on Route 256 is restricted to a right-in/left-in/right-out access and one of the northeast gas station driveway's is restricted to a right-in/right-out by installing a median on Route 256. Finally, the Ridgetop Drive improvement improves the existing road cross-section and provides access to the southwest gas station and any future development in the northwest corner

A concept sketch of this alternative is shown in Figure 13.

### 4.1.2 Single-lane roundabout

This alternative reconfigures the intersection to a single-lane roundabout. The access to the southwest gas station on Route 256 is restricted to a right-in/right-out. Similar to the previous alternative, the Ridgetop Drive improvement will still improve the existing road cross-section and provides access to the southwest gas station and any future development in the northwest corner. The roundabout is assumed to have a 150 foot diameter with 16 ' circulating lanes. The roundabout was concepted to accommodate a WB-67 tractor trailer using AutoTurn software

A concept sketch of this alternative is shown in Figure 14.

Figure 13. US 11: Minimally Managed Improvements


Figure 14. US 11:Single-Lane Roundabout

4.1.3 Alternative Summary

The anticipated AM and PM 2045 operational results can be found in Table 5
Of all the alternatives examined, the single-lane roundabout provides the greatest operational and safety benefit. Overall intersection delay decreases up to $70 \%$ and crashes are anticipated to reduce by up to $60 \%$. The operations for the single-lane roundabout are improved, however queues traveling westbound in the AM on Route 256 extend up to 249 feet. Similar crash benefits are expected at $60 \%$ but less rear-ends are expected at the I-81 southbound ramp and Route 256 intersection. Finally, the minimally managed improvement is expected to improve operations up to $20 \%$. Safety benefits are expected to be up to $15 \%$ for enhanced signal conspicuity at the main intersection and up to $60 \%$ reduction in access management related crashes at the two gas station driveways.

Table 5. US 11: 2045 Operational Results for Alternative

| Direction | Lane Group | No Improvements |  |  | Minimally Managed |  |  | Single-lane Roundabout |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue <br> Length <br> (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue Length (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | $\begin{aligned} & \text { Queue } \\ & \text { Length } \\ & \text { (ft) } \end{aligned}$ |
| AM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Ridgetop Drive Eastbound | Left | 20.6 | c | - | 15.9 | B | - | 8.2 | A | 9 |
|  | Through | 20.6 | c | 18 | 15.9 | B | 22 | 8.2 | A | 9 |
|  | Right | 20.6 | c | - | 15.9 | B | - | 8.2 | A | 9 |
| Route 256 Westbound | Left | 31.0 | c | 226 | 40.6 | D | 349 | 12.7 | B | 192 |
|  | Through | 31.0 | c | 226 | 40.6 | D | 349 | 12.6 | B | 192 |
|  | Right | 21.9 | c | 0 | 22.9 | c | 7 | 12.8 | B | 192 |
| US 11 Northbound | Left | 40.7 | D | 18 | 24.8 | c | 3 | 9.1 | A | 83 |
|  | Through | 127.9 | F | 261 | 36.0 | c | 172 | 9.3 | A | 83 |
|  | Right | 41.5 | D | 13 | 27.2 | c | 0 | 9.4 | A | 83 |
| US 11 Southbound | Left | 54.3 | D | 265 | 22.7 | c | 168 | 16.5 | B | 235 |
|  | Through | 27.1 | c | 186 | 24.2 | c | 178 | 16.5 | B | 235 |
|  | Right | 27.1 | c | 186 | 24.2 | c | 178 | 16.2 | B | 235 |
| Gas Station | Left | 47.1 | D | 0 | N/A - Vehicles routed to Ridgetop Drive |  |  | N/A - Vehicles routed to RidgetopDrive |  |  |
|  | Through | 47.1 | D | - |  |  |  |  |  |  |
|  | Right | 47.1 | D | 0 |  |  |  |  |  |  |
| Overall |  | 47.4 | D | - | 30.1 | c | - | 13.1 | B | - |
| PM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Ridgetop Drive Eastbound | Left | 38.4 | D | - | 25.0 | c | - | 6.8 | A | 5 |
|  | Through | 38.4 | D | 18 | 25.0 | c | 23 | 6.8 | A | 5 |
|  | Right | 38.4 | D | - | 25.0 | c | - | 6.8 | A | 5 |
| Route 256 Westbound | Left | 45.2 | D | 226 | 42.0 | D | 146 | 9.3 | A | 98 |
|  | Through | 45.2 | D | 226 | 42.0 | D | 146 | 9.3 | A | 98 |
|  | Right | 35.7 | D | 0 | 51.8 | D | 57 | 9.7 | A | 98 |
| US 11 Northbound | Left | 28.0 | c | 18 | 20.4 | c | 4 | 12.4 | B | 170 |
|  | Through | 32.3 | c | 261 | 24.9 | c | 151 | 12.5 | B | 170 |
|  | Right | 30.5 | c | 13 | 22.8 | c | 64 | 12.5 | B | 170 |
| US 11 Southbound | Left | 16.7 | в | 265 | 11.4 | в | 146 | 12.8 | B | 191 |
|  | Through | 15.4 | в | 186 | 9.8 | A | 135 | 12.8 | B | 191 |
|  | Right | 15.4 | B | 186 | 9.8 | A | 135 | 12.6 | B | 191 |
| Gas Station | Left | 57.1 | E | 0 | N/A - Vehicles routed to Ridgetop Drive |  |  | N/A - Vehicles routed to Ridgetop Drive |  |  |
|  | Through | 57.1 | E | - |  |  |  |  |  |  |
|  | Right | 57.1 | E | 0 |  |  |  |  |  |  |
| Overall |  | 28.3 | c | - | 25.4 | c | - | 11.7 | B | - |

### 4.2 I-81 and Route 256 interchange

Apart from one alternative, the alternatives for Route 256 and the ramps can be implemented individually and do not rely on the construction of another. The study team reviewed and decided not to advance alternatives for a partial reroute roundabout scenario for the southbound $1-81$ ramp, a diverging diamond interchange, and a single point urban interchange. Although these ideas had positive operational and safety benefits, the cost to construct them compared to the selected alternatives was high, and the study team indicated that these were not contextually sensitive solutions. The study team advanced the following alternatives for detailed reviewed of the interchange:

### 4.2.1 Single-lane teardrop roundabout

This alternative reconfigures either ramp intersection to a single-lane teardrop style roundabout. These improvements are not anticipated to impact the bridge and are considered projects of independent utility. Both roundabouts incorporate the funded improvements. Both roundabouts are assumed to have a 160 foot diameter with 16 ' circulating lanes. The roundabouts were concepted to accommodate a WB- 67 tractor trailer using AutoTurn software. It should be noted that the northbound ramp roundabout could be increased in size to accommodate larger trucks better. A concept sketch for each ramp node of this alternative is shown in Figure 15.

### 4.2.2 Three-lane bridge deck with left-turn lane

This alternative widens the bridge deck to three lanes and reconfigures both ramp intersections with Route 256. The number of through lanes would remain the same, however a left-turn lane would be provided for both ramps to allow refuge for vehicles making a left onto $1-81$. This improvement would incorporate the funded improvements. A concept sketch of this alternative is shown in Figure 16.

### 4.2.3 Alternative Summary

The anticipated operational results for both the $1-81$ southbound ramp and $1-81$ northbound ramp on Route 256 can be found in Tables 6 and 7 , respectively.

The roundabouts provide the most operational and safety benefit. Both intersections would expect significant operational improvements. The southbound $1-81$ ramp is anticipated to see the worst peak hour delays decrease from 60.0 seconds/vehicle to 11.7 seconds/vehicle in the PM peak hour. The northbound $1-81$ ramp would see the worst peak hour delay decrease from 40.7 seconds/vehicle to 9.1 seconds/vehicle in the PM peak hour. Furthermore, the queues between the bridges reduce which also reduces the risk of rear end crashes. Finally, the bridge widening does improve overall delay and queue lengths, however the crash benefit is less than the roundabout, which is an anticipated $15 \%$ crash reduction compared to the $60 \%$ crash reduction of a roundabout.

Figure 15. I-81 Interchange: Single-Lane Teardrop Roundabout


Figure 16. I-81 Interchange: Three-Lane Bridge

4.2.4 Corridor Evaluation and Phasing

All proposed alternatives will enhance the operations and safety of the corridor. However, implementation of the alternatives together at a corridor level must be considered. The most operational beneficial and safest corridor alternative would be roundabouts at all three locations since no queuing is anticipated to back-up into an upstream roundabout in the AM and PM peak hours. If US 11 and Route 256 is improved with the minimally managed scenario and the bridge is widened, operations will be improvement but queuing may still back-up into each intersection during the AM or PM peak hours between Route 11 and the southbound I-81 ramp on Route 256. The distance between these two intersections are about 300 feet, the AM controlling queue is at Route 11 and Route 256 in the westbound direction at 349 feet. The PM controlling queue is at the southbound I-81 ramp and Route 256 in the eastbound direction at 370 feet. This issue will be more problematic with a corridor scenario where there is a roundabout at either node and the minimally managed or bridge widening is implemented since the queue may back into the roundabout. However, more importantly, the no improvement scenario showed that the southbound I-81 ramp and Route 256 intersection is over-capacity meaning that this intersection with no improvement would significantly impact the operations of a roundabout at Route 11 and Route 256 . Therefore, it is recommended that if the roundabout at Route 11 and Route 256 is pursued, the bridge widening or roundabout at the southbound I-81 ramp is implemented first.

Table 7. 1-81 Interchange: Operational Results for Alternatives (Northbound)

| Direction | Lane Group | No Improvements |  |  | Roundabout |  |  | Three-Lane Bridge |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue <br> Length <br> (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue Length (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue Length (ft) |
| AM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Route 256 <br> Eastbound | Left | 45.8 | D | 252 | 6.9 | A | 0 | 12.5 | в | 49 |
|  | Through | 45.8 | D | 252 | 6.9 | A | 0 | 2.7 | A | 36 |
| Route 256 Westbound | Through | 19.6 | B | 372 | 10.2 | B | 141 | 25.9 | C | 395 |
|  | Right | 13.7 | B | 43 | 10.2 | B | 103 | 15.3 | B | 49 |
| 1-81 <br> Northbound | Left | 89.6 | F | 451 | 12.5 | B | 137 | 49.3 | D | 334 |
|  | Through | 89.6 | F | 451 | 12.3 | B | 137 | 49.3 | D | 334 |
|  | Right | 89.6 | F | 451 | 12.8 | B | 137 | 49.3 | D | 334 |
| Overall |  | 60.0 | D | 451 | 9.9 | A | - | 23.7 | c | - |
| PM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Route 256 Eastbound | Left | 31.6 | c | 371 | 12.5 | B | 0 | 3.2 | A | 22 |
|  | Through | 31.6 | c | 371 | 12.7 | B | 0 | 4.1 | A | 145 |
| Route 256 Westbound | Through | 13.3 | B | 229 | 6.5 | A | 62 | 17.3 | B | 252 |
|  | Right | 11.0 | B | 35 | 6.5 | A | 46 | 13.2 | B | 45 |
| 1-81 <br> Northbound | Left | 94.6 | F | 461 | 18.6 | B | 168 | 36.7 | D | 210 |
|  | Through | 94.6 | F | 461 | 18.1 | B | 168 | 36.7 | D | 210 |
|  | Right | 94.6 | F | 461 | 18.5 | B | 168 | 36.7 | D | 210 |
| Overall |  | 36.9 | D | - | 11.6 | в | - | 14.4 | в | - |

Table 6. I-81 Interchange: Operational Results for Alternatives (Southbound)

| Direction | Lane Group | No Improvements |  |  | Roundabout |  |  | Three-Lane Bridge |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue Length (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | Queue length (ft) | $\begin{aligned} & \text { Delay } \\ & \text { (Sec/veh) } \end{aligned}$ | LOS | $\begin{aligned} & \text { Queue } \\ & \text { Length } \\ & \text { (ft) } \end{aligned}$ |
| AM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Route 256 Eastbound | Through | 5.7 | A | 52 | 7.8 | A | 65 | 17.1 | B | 164 |
|  | Right | 0.2 | A | 0 | 7.8 | A | 33 | 8.9 | A | 15 |
| Route 256 <br> Westbound | Left | 53.4 | D | 675 | 10.9 | B | 0 | 6.4 | A | 50 |
|  | Through | 53.4 | D | 675 | 10.8 | B | 0 | 2.7 | A | 46 |
| $\begin{gathered} \text { I-81 } \\ \text { Southbound } \end{gathered}$ | Left | 98.7 | F | 431 | 21.8 | C | 229 | 42.0 | D | 287 |
|  | Through | 98.7 | F | 431 | 21.1 | c | 229 | 42.0 | D | 287 |
|  | Right | 98.7 | F | 431 | 21.4 | c | 229 | 42.0 | D | 287 |
| Overall |  | 51.7 | D | - | 12.9 | B | - | 17.2 | B | - |
| PM Peak Hour |  |  |  |  |  |  |  |  |  |  |
| Route 256 Eastbound | Through | 15.7 | B | 152 | 12.3 | B | 161 | 26.8 | C | 370 |
|  | Right | 3.3 | A | 5 | 10.8 | B | 56 | 5.3 | A | 7 |
| Route 256 Westbound <br> Westbound | Left | 70.5 | E | 476 | 7.3 | A | 0 | 16.1 | B | 109 |
|  | Through | 70.5 | E | 476 | 7.2 | A | 0 | 3.5 | A | 37 |
| $\begin{gathered} 1-81 \\ \text { Southbound } \end{gathered}$ | Left | 105.8 | F | 686 | 20.4 | c | 302 | 52.8 | D | 438 |
|  | Through | 105.8 | F | 686 | 20.0 | c | 302 | 52.8 | D | 438 |
|  | Right | 105.8 | F | 686 | 20.4 | c | 302 | 52.8 | D | 438 |
| Overall |  | 60 | E |  | 13.3 | B |  | 27.9 | c |  |

## 5. Conceptual Level Construction Costs and Impacts

The study team developed construction level cost estimate ranges using the Statewide Planning Tool (SPLCE) and VDOT unit cost averages. Costs in the tables below do include detailed construction and preliminary engineering (PE) estimates. The study team evaluated the right-of-way impacts qualitatively and used the SPLCE recommended right-ofway and utility percentage based on the conceptual sketches and parcel lines.

### 5.1 Intersection of US Route 11 and Route 256

Table 8 summarizes the construction cost ranges and right-of-way impacts.
Table 8. US 11: Construction Cost Ranges and Right-of-Way Impacts

|  | No Improvements | Minimally Managed | Single-lane Roundabout |
| :---: | :---: | :---: | :---: |
| Estimated Cost <br> (Construction + PE) | - | $\$ 2,620,000$ | $\$ 4,260,000$ |
| Right-of-way Impacts | - | None to minimal takes | Minimal to moderate <br> takes |

All improvements assume that Ridgetop Drive reconstruction would occur, therefore, those costs are included. The Ridgetop Drive improvement will also impact nearby properties since the road is being widening and its elevation adjusted. The southwest gas station and northwest property would be impacted. The minimally managed improvement is anticipated to be the least costly since the majority of work is only on Route 11 . The traffic signal will need to be reconstructed. The roundabout is more costly since the amount of pavement and median construction that would need to occur increases cost. The anticipated maintenance of traffic would be a large cost item due to the construction method involved with roundabout construction.

### 5.2 I-81 and Route 256 interchange

Table 9 summarizes the construction cost ranges and right-of-way impacts.
Table 9. I-81 Interchange: Construction Cost Ranges and Right-of-Way Impacts

|  | No Improvements | Three-Lane Bridge | Roundabout |
| :---: | :---: | :---: | :---: |
| Estimated Cost <br> (Construction + PE) | - | $\$ 16,500,000$ | $\$ 5.0 \mathrm{M}$ to $\$ 7.0 \mathrm{M}$ each |
| Right-of-way Impacts | - | None to minimal takes | Minimal to moderate <br> takes at $181 \mathrm{SB} /$ Rte 256 |

Both advanced improvements should have minimal right-of-way impact since most work should occur within the interchange area. The southbound I-81 roundabout alternative is anticipated to have some impact to the BP gas station and the southwest corner of the intersection. The bridge widening and the combination of the roundabouts may have similar construction cost, however, the roundabouts can be implemented in phases, if both are advanced for funding his independent utility advantage may increase funding chances or decrease traffic disruptions during construction. Furthermore, the roundabouts construction does not preclude from a future bridge widening or vice versa. Finally, both improvements are anticipated to disrupt traffic during construction, however the bridge widening does have a high risk of lane closures on $\mathrm{I}-81$ which increases construction timeline and cost.

## 6. Public Involvement Results

The community provided feedback was requested via a virtual survey and in-person public meeting. The virtual survey was conducted between December 3rd and December 23rd, 2021. The in-person public meeting was conducted in person at BRCC on March 7, 2022. Below is a summary of the public comments:

- 447 responses were received for the virtual survey
- $53 \%$ of respondents live/work within the study area
- Community feedback generally agreed with the identified issues from the study team
- Most respondents agreed that doing no improvements was not acceptable


### 6.1 Intersection of US Route 11 and Route 256

Figure 17 summarizes the average rating from the virtual survey. Comments from the public meeting are summarized in this section.

Most respondents and comments at the in-person meeting agreed that something should occur. The roundabout was rated most favorably with a 3.36 average score out of 5 , whereas the minimally managed option received a 2.86 average score. Comments during the meeting felt that reducing access to the gas station driveways and improving Ridgetop Drive would improve safety. As well, there was a general misunderstanding of how a roundabout works, which was explained further by study team members during the in-person meeting.

### 6.2 6.2 I-81 and Route 256 interchange

Figure 18 summarizes the average rating from the virtual survey. Comments from the public meeting are summarized in this section

Most respondents and comments at the in-person meeting agreed that something should occur. The bridge was rated most favorably with a 3.60 average score out of 5 , whereas both roundabouts received more than a 3.00 average score. Comments during the meeting and on the survey liked the bridge widening but felt that the bridge widening should consider more lanes. During the in-person meeting, community feedback generally did not disagree or agree with multiple roundabouts on the corridor, but at least one roundabout on the segment was viewed favorably.

Figure 17. US 11: Metroquest Summary

No Build


Minimally Managed


Single-lane Roundabout


Figure 18. I-81 Interchange: Metroquest Summary


## 7. Conclusions and Recommendations

The study highlighted several issues within the study area that would be addressed by the alternatives. Based on stakeholder input and community involvement, there was a consensus that improvements were needed within the study area to enhance safety and improve operations. Depending on the funding source, such as SMART SCALE, lowe cost improvements with high benefits tend to score better and receive funding. The roundabouts at all locations generally have a high benefit compared to the other advanced alternatives, and provide independent utility that could permit them to be submitted for funding as separate projects. However, based on stakeholder and community feedback, it may be best to consider an implementation plan of one roundabout at the most favorable location on the corridor to monitor performance and improve community support. If the bridge widening is pursued, a mor detailed construction requirements review (such as superstructure/substructure performance and I-81 maintenance of traffic risks) is recommended to help reduce cost risk and increase competitiveness. The bridge widening could still be mplemented with the construction of one or both of the roundabout concepts.

1. Appendix A: Route 256 Area Plan - Base Year Volumes and Future Growth Rates

## Michael Baker

## Memorandum

## I N T ERNATIONAL

| TO: | Adam Campbell, PLA, VDOT | DATE: | May 26, 2021 |
| :--- | :--- | :--- | :--- |
|  | Matt Bond, P.E., VDOT |  |  |$\quad$ SUBJECT: $\quad$| Small Area Study Exit 235 and Route |
| :--- |
| FROM: |
| Daniel Scolese, P.E. |

## Purpose

The purpose of this memorandum is to document the base year volumes and future growth rate development for the Exit 235 and Route 256 Small Area Study.

## Study Area:

The study area for the Exit 235 and Route 256 Small Area Study as shown in Figure 1 is located in Augusta County along Route 256 between US 11 and the Triangle Drive.

Figure 1: Exit 235 and Route 256 Small Area Study


The intersections along Route 256 that will be analyzed as part of the study area are as follows:

- US 11 and Route 256
- Route 256 and I-81 Southbound Ramp
- Route 256 and I-81 Northbound Ramp
- Route 256 and Triangle Drive


## Base Year Development

In response to IIM TMPD 7.0, base year volumes were developed for the study intersections due to COVID-19 traffic impacts. Traffic counts for the following intersections were collected on November $14^{\text {th }}, 2017$ :

- US 11 and Route 256
- Route 256 and I-81 Southbound Ramp
- Route 256 and I-81 Northbound Ramp

Traffic counts were collected for Route 256 and Triangle Drive on April 13, 2021.
Figure 2 shows the unbalanced turning movement counts for the study area
Figure 2: Unbalanced Turning Movement Counts


Table 1 summarizes the Statewide Planning System (SPS) historical data for each segment.

Table 1: SPS AADT Data

| Roadway | From | To | 2005 | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 | 2018 | 2019 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US 11 | Rockingham <br> County Line | Sidney Gap Road | 5,683 | 5,840 | 5,557 | 5,722 | 5,370 | 4,646 | 4,584 | 4,606 | 5,513 | 5,624 | 5,860 | 5,542 | 5,666 | 5,643 | 6,466 |
| Route 256 | US 11 | I-81 | 9,009 | 9,257 | 7,209 | 7,423 | 6,967 | 7,100 | 7,005 | 7,038 | 8,849 | 9,028 | 9,406 | 8,267 | 8,452 | 8,087 | 8,097 |
| Route 256 | I-81 | SR 2002 | 9,568 | 9,831 | 9,216 | 8,769 | 8,762 | 8,804 | 8,969 | 9,136 | 9,332 | 9,215 | 9,261 | 9,908 | 10,156 | 10,166 | 10,221 |
| Route 256 | SR 2002 | Route 276 | 9,568 | 9,831 | 9,216 | 8,769 | 8,762 | 8,804 | 8,969 | 9,136 | 9,332 | 9,215 | 9,261 | 9,908 | 10,156 | 10,166 | 10,221 |
| I-81 | Toll Gate Road | Route 256 | 49,048 | 49,674 | 49,466 | 45,782 | 46,275 | 47,533 | 47,117 | 48,239 | 48,820 | 50,115 | 52,736 | 55,198 | 56,310 | 54,755 | 56,542 |
| I-81 | Route 256 | Rockingham <br> County Line | 47,975 | 50,059 | 50,089 | 47,488 | 48,473 | 49,202 | 48,120 | 49,221 | 49,802 | 50,340 | 53,549 | 56,061 | 56,931 | 55,510 | 56,660 |

Table 2 summarizes the available Continuous Count Station data for Route 256 east of Route 276, and the I-81 stations north and south of the Route 256 interchange. This is real-time data that can be used determine regional effects.

Table 2: SPS AADT Data

| Continous Count Station Data: Average Annual Vehicles Per Day |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road Name | Location | Station ID | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 1 8}$ | $\mathbf{2 0 1 9}$ | $\mathbf{2 0 2 0}$ |
| Route 256 | East of Route 276 | 80128 | 5,981 | 5,969 | 6,172 | 5,736 |
| 1-81 Southbound | North of Route 256 | 180027 | 27,833 | 26,763 | 28,079 | 23,623 |
| 1-81 Northbound | South of Route 256 | 80299 | 29,417 | 28,069 | 28,667 | 24,291 |

Based on the Continuous Count Station data for Route 256, COVID did impact the volumes along the segment, however the 2017 and 2019 volumes remain relatively unchanged. The SPS data also confirms that Route 256 has seen minimal increases in traffic since 2017. Furthermore, based on the assumption that November 2017 is a reasonable base year, the April 2021 turn movement counts compared to the November 2017 turn movement counts are within a reasonable margin of each other. Although seasonality is an aspect, it may also signify that volumes are returning to pre-COVID conditions.

Although no Continuous Count Stations are present on the I-81 ramps, the stations north and south of the Route 256 interchange also show that COVID-19 did impact volumes. Similar to Route 256 , the difference between the 2017 traffic volumes and the 2019 traffic volumes are within a reasonable margin of each other.

Finally, the only available data on US 11 is the SPS data. The AADT along US 11 does increase from 5,700 vehicles per day in 2017 to about 6,500 vehicles per day by 2019. However, looking back to previous years, the AADT has remained relatively unchanged. Although the slight increase could be due to other outside causes, a review of aerial imagery along the US 11 SPS segment does not show any changes.

Therefore, it is recommended to use the turning movement volumes from the November 2017 traffic counts. The base year traffic volumes for the study use these to balance the turning movements at the intersection of Route 256 and Triangle Drive (collected in April, 2021). Figure 3 shows the resulting base year volumes to be used for the Exit 235 and Route 256 Small Area Study.

Figure 3: Recommended Base Year Volumes


## Growth Rate Development

The following sources of data were reviewed to determine growth rates to apply to the existing traffic volumes to forecast to 2045:

- Statewide Planning System Data from Table 1
- Staunton-Augusta-Waynesboro MPO Model
- March 2021 - I-81 Weyers Cave Truck Climbing Lane Traffic Growth and Forecast Memo
- August 2015 Airport Road Traffic Impact Analysis

Table 3 summarizes the SPS linear growth rates for each segment within the study corridor.

Table 3: SPS Linear Growth Rates

| Roadway | From | To | SPS Growth Rate |
| :---: | :---: | :---: | :---: |
| US 11 | Rockingham County Line | Sideny Road | $0.53 \%$ |
| Route 256 | US 11 | I-81 | $1.55 \%$ |
| Route 256 | I-81 | SR 2002 | $1.74 \%$ |
| Route 256 | SR 2002 | Route 276 | $0.67 \%$ |
| I-81 | Toll Gate Road | Route 256 | $1.18 \%$ |
| I-81 | Route 256 | Rockingham County Line | $1.77 \%$ |

Table 4 summarizes the SAWMPO Model outputs for 2018 and 2045, with the linear growth rates.
Table 3: SAWMPO Model: Linear Growth Rates

| LINK_ID | Description | 2018 | $\mathbf{2 0 4 5}$ | Growth Rate |
| :---: | :---: | :---: | :---: | :---: |
| 169307 | US 11 North of Route 256 | 8110 | 10029.88 | $0.88 \%$ |
| 169306 | US 11 South of Route 256 | 7091 | 12060.66 | $2.60 \%$ |
| 169314 | I-81 SB on Route 256 | 3507.75 | 5937.9 | $2.57 \%$ |
| 169308 | I-81 SB off Route 256 | 5189.55 | 3879.26 | $-0.94 \%$ |
| 169303 | I-81 NB on Route 256 | 5130.69 | 4151.59 | $-0.71 \%$ |
| 169312 | I-81 SB off Route 256 | 3499.53 | 4949 | $1.53 \%$ |
| 127826 | Route 256 east of Triangle Drive | 12228.82 | 12675.63 | $0.14 \%$ |

The March 2021 I-81 Weyers Cave Truck Climbing Lane Traffic Growth and Forecast Memo summarizes the growth rates for mainline I-81 and the ramps within the study area. Since the ramp termini are associated with the Exit 235 and Route 256 Small Area Study, the memo recommends a $2.00 \%$ linear growth rate be applied to a daily ramp volume estimate by dividing the 2017,12 -hour turning movement counts by 0.75 .

Finally, the August 2015 Airport Road Traffic Impact Analysis used a 0.5\% annual linear background growth rate for all turning movements. The memo also summarizes the anticipated growth from the expansion. The outlined growth is aggressive, however based on feedback from August County and the Central Shenandoah Planning District Commission, the airport has seen increased air traffic prior to COVID-19. The region is actively interested in promoting the airport and expanding, therefore, the $2.00 \%$ linear growth rate methodology for the ramps and $1 \%$ background linear growth rate will provide reasonable growth expectations on the Route 256 segment heading east towards the airport from I-81.

After reviewing the following data with Staunton District, Augusta County, and Central Shenandoah Planning District Commission on May 10, 2021, the following agreed upon linear annual growth rates will be applied to the existing turning movements to forecast the 2045 volumes for the Exit 235 and Route 256 Small Area Study:

- 1\% background linear growth rate applied to Route 256.
- Apply the same methodology for the I-81 ramp Volumes as the March 2021 Memo.
- $2.00 \%$ linear growth rate be applied to the daily ramp volume estimate by dividing the 2017, 12hour turning movement counts by 0.75 .
- The additional volume will be carried back towards the east on Route 256 to account for the higher growth associated with the airport and planned improvements to the east.
- $1 \%$ linear growth rate applied to US 11.
- Zero or no growth for the northbound approach of Triangle Drive.
- Site Traffic ITE Calculation for the funded Park and Ride Lot entrance at Triangle Drive using ITE Trip Generation Code 090 - Park and Ride Lot with Bus or Light Rail.
- Site Traffic ITE Calculation for the Landings Drive Weyers Caver Apartment Complex using the highest of the two ITE Trip Generation Codes 221 - Multifamily Housing (Mid-Rise) or 231 - Mid Rise with $1^{\text {st }}$ Floor Commercial.

2. Appendix B: Synchro Report - Existing Conditions

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cane/z(z民d)


Analysis Period (min)
15
c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cale/z(2民\&)

|  | $\dagger$ | $\downarrow$ | 4 | $\dagger$ | ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR | NEL | NER | NER2 |
| Lane ${ }^{\text {\% }}$ (onfigurations | $\uparrow$ |  | M |  | 「 |
| Trafic Volume (vph) | 166 | 11 | 2 | 11 | 21 |
| Future Volume (vph) | 166 | 11 | 2 | 11 | 21 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 10.2 |  | 9.4 |  | 9.4 |
| Lane Util. Factor | 1.00 |  | 1.00 |  | 0.95 |
| Frt | 0.99 |  | 0.86 |  | 0.85 |
| FIt Protected | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (prot) | 1788 |  | 1615 |  | 1461 |
| Flt Permitted | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (perm) | 1788 |  | 1615 |  | 1461 |
| Peak-hour factor, PHF | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Adj. Flow (vph) | 191 | 13 | 2 | 13 | 24 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 18 |
| Lane Group Flow (vph) | 204 | 0 | 1 | 0 | 1 |
| Heavy Vehicles (\%) | 5\% | 9\% | 0\% | 0\% | 5\% |
| Turn Type | NA |  | Perm |  | Perm |
| Protected Phases | 6 |  |  |  |  |
| Permitted Phases |  |  | 3 |  | 3 |
| Actuated Green, G (s) | 36.0 |  | 3.0 |  | 3.0 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 36.0 |  | 3.0 |  | 3.0 |
| Actuated g/C Ratio | 0.36 |  | 0.03 |  | 0.03 |
| Clearance Time (s) | 10.2 |  | 9.4 |  | 9.4 |
| Vehicle Extension (s) | 4.0 |  | 2.0 |  | 2.0 |
| Lane Grp Cap (vph) | 643 |  | 48 |  | 43 |
| v/s Ratio Prot | 0.11 |  |  |  |  |
| v/s Ratio Perm |  |  | 0.00 |  | c0.00 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.32 |  | 0.01 |  | 0.01 |
| Uniform Delay, d1 | 23.1 |  | 47.1 |  | 47.1 |
| Progression Factor | 1.00 |  | 1.00 |  | 1.00 |
| Incremental Delay, d2 | 1.3 |  | 0.0 |  | 0.0 |
| Delay (s) | 24.4 |  | 47.1 |  | 47.1 |
| Level of Service | C |  | D |  | D |
| Approach Delay (s) | 28.4 |  | 47.1 |  |  |
| Approach LOS | C |  | D |  |  |
| Intersection Summary |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp


HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)
06/23/2021


|  | $\rightarrow$ |  |  | $4 \quad 4$ |  | 7 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | $\hat{1}$ |  |  | $\uparrow$ | M |  |  |  |
| Traffic Volume (veh/h) | 265 | 60 | 28 | 633 | 50 | 10 |  |  |
| Future Volume (Veh/h) | 265 | 60 | 28 | 633 | 50 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |  |  |
| Hourly flow rate (vph) | 298 | 67 | 31 | 711 | 56 | 11 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |
| Walking Speed (tt/s) |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type | None |  |  | None |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |
| Upstream signal (ft) | 899 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |
| VC , conflicting volume |  |  | 365 |  | 1104 | 332 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu, unblocked vol |  |  | 365 |  | 1104 | 332 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 6.7 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.9 | 3.8 |  |  |
| p0 queue free \% |  |  | 97 |  | 71 | 98 |  |  |
| cM capacity (veh/h) |  |  | 1183 |  | 192 | 613 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 |  |  |  |  |  |
| Volume Total | 365 | 742 | 67 |  |  |  |  |  |
| Volume Left | 0 | 31 | 56 |  |  |  |  |  |
| Volume Right | 67 | 0 | 11 |  |  |  |  |  |
| cSH | 1700 | 1183 | 216 |  |  |  |  |  |
| Volume to Capacity | 0.21 | 0.03 | 0.31 |  |  |  |  |  |
| Queue Length 95th (ft) | 0 | 2 | 32 |  |  |  |  |  |
| Control Delay (s) | 0.0 | 0.7 | 29.0 |  |  |  |  |  |
| Lane LOS |  | A | D |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.7 | 29.0 |  |  |  |  |  |
| Approach LOS |  |  | D |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 65.8\% |  | CU Level | Service | C | C |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cane/z(z民d)


Analysis Period (min)
15
c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cane/z(z民d)


HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp
06/23/2021


HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)
06/23/2021



Queues
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cale/z(zed)

|  | $\rightarrow$ |  |  | , | $\dagger$ | \% |  | $\dagger$ | 4 | $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT | NEL | NER2 |
| Lane Group Flow (vph) | 13 | 432 | 154 | 8 | 174 | 148 | 232 | 204 | 20 | 19 |
| v/c Ratio | 0.02 | 0.93 | 0.22 | 0.03 | 0.44 | 0.28 | 0.63 | 0.29 | 0.06 | 0.06 |
| Control Delay | 25.8 | 54.6 | 0.7 | 31.4 | 38.0 | 1.3 | 30.4 | 21.9 | 0.4 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.4 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.8 | 54.6 | 0.7 | 31.4 | 38.0 | 1.4 | 30.9 | 21.9 | 0.4 | 0.4 |
| Queue Length 50th (ft) | 6 | ~329 | 0 | 4 | 97 | 0 | 101 | 87 | 0 | 0 |
| Queue Length 95th (ft) | 20 | \#483 | m0 | 16 | 155 | 0 | 155 | 136 | 0 | 0 |
| Internal Link Dist (ft) | 467 | 317 |  |  | 841 |  |  | 1001 | 128 |  |
| Turn Bay Length (ft) |  |  | 240 | 185 |  | 185 | 365 |  |  |  |
| Base Capacity (vph) | 585 | 465 | 714 | 260 | 394 | 534 | 369 | 711 | 382 | 369 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 36 | 16 | 0 | 8 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.02 | 0.93 | 0.22 | 0.03 | 0.44 | 0.30 | 0.66 | 0.29 | 0.05 | 0.05 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |
| m Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp


Queues
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)

|  | $\rightarrow$ | $\leftarrow$ | $\dagger$ |
| :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBT |
| Lane Group Flow (vph) | 382 | 768 | 313 |
| v/c Ratio | 0.76 | 0.80 | 0.83 |
| Control Delay | 19.8 | 24.9 | 46.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 |
| Total Delay | 19.8 | 24.9 | 46.4 |
| Queue Length 50th (tt) | 99 | 362 | 131 |
| Queue Length 95th (ft) | m\#159 | 536 | \#257 |
| Internal Link Dist (ft) | 724 | 819 | 951 |
| Turn Bay Length (ft) |  |  |  |
| Base Capacity (vph) | 502 | 963 | 400 |
| Starvation Cap Reductn | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.76 | 0.80 | 0.78 |
| Intersection Summary |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |
| $m$ Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |

Queues
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cale/z(zed)

|  | $\rightarrow$ |  |  | 4 | $\dagger$ | $\rangle$ | ( | - | 4 | $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT | NEL | NER2 |
| Lane Group Flow (vph) | 4 | 186 | 207 | 12 | 163 | 277 | 266 | 256 | 15 | 10 |
| v/c Ratio | 0.01 | 0.70 | 0.36 | 0.04 | 0.32 | 0.42 | 0.55 | 0.27 | 0.04 | 0.02 |
| Control Delay | 24.8 | 42.1 | 2.3 | 28.2 | 29.0 | 4.3 | 20.2 | 14.5 | 0.1 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.2 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.8 | 42.1 | 2.3 | 28.2 | 29.0 | 4.6 | 20.4 | 14.5 | 0.1 | 0.1 |
| Queue Length 50th (ft) | 2 | 79 | 0 | 4 | 65 | 0 | 64 | 61 | 0 | 0 |
| Queue Length 95th (ft) | 9 | m130 | m12 | 20 | 136 | 42 | \#176 | 149 | 0 | 0 |
| Internal Link Dist (ft) | 467 | 317 |  |  | 841 |  |  | 1001 | 128 |  |
| Turn Bay Length (ft) |  |  | 240 | 185 |  | 185 | 365 |  |  |  |
| Base Capacity (vph) | 332 | 277 | 584 | 309 | 509 | 664 | 486 | 941 | 467 | 463 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 81 | 22 | 0 | 87 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.01 | 0.67 | 0.35 | 0.04 | 0.32 | 0.48 | 0.57 | 0.27 | 0.04 | 0.02 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp


Queues
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)

|  | $\rightarrow$ | $\leftarrow$ | $\dagger$ |
| :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBT |
| Lane Group Flow (vph) | 666 | 493 | 267 |
| v/c Ratio | 0.77 | 0.66 | 0.67 |
| Control Delay | 11.2 | 23.4 | 23.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 |
| Total Delay | 11.2 | 23.4 | 23.8 |
| Queue Length 50th (tt) | 63 | 174 | 64 |
| Queue Length 95th (ft) | m\#108 | \#347 | 132 |
| Internal Link Dist (ft) | 724 | 819 | 951 |
| Turn Bay Length (ft) |  |  |  |
| Base Capacity (vph) | 861 | 746 | 494 |
| Starvation Cap Reductn | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.77 | 0.66 | 0.54 |
| Intersection Summary |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |
| $m$ Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |

3. Appendix C: Synchro Report - Future No-Build Conditions

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers CaNQ/Ragerd)

|  | * | $\rightarrow$ |  | 4 | 5 | $\bullet$ | 4 | $\cdots$ | 4 | $\dagger$ | $p$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR | SBL |
| Lane Configurations |  | $\dagger$ |  |  |  | 4 | 「 |  | ${ }^{7}$ | 4 | 「 | ${ }^{1}$ |
| Traffic Volume (vph) | 2 | 5 | 4 | 387 | 14 | 0 | 179 | 6 | 1 | 188 | 163 | 256 |
| Future Volume (vph) | 2 | 5 | 4 | 387 | 14 | 0 | 179 | 6 | 1 | 188 | 163 | 256 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 7.1 |  |  |  | 7.1 | 7.1 |  | 10.2 | 10.2 | 10.2 | 10.2 |
| Lane Util. Factor |  | 1.00 |  |  |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.95 |  |  |  | 1.00 | 0.85 |  | 1.00 | 1.00 | 0.85 | 1.00 |
| Flt Protected |  | 0.99 |  |  |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 |
| Satd. Flow (prot) |  | 1788 |  |  |  | 1722 | 1524 |  | 1805 | 1810 | 1524 | 1703 |
| Fit Permitted |  | 0.95 |  |  |  | 0.75 | 1.00 |  | 0.60 | 1.00 | 1.00 | 0.27 |
| Satd. Flow (perm) |  | 1709 |  |  |  | 1358 | 1524 |  | 1149 | 1810 | 1524 | 489 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 2 | 6 | 5 | 440 | 16 | 0 | 203 | 7 | 1 | 214 | 185 | 291 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 130 | 0 | 0 | 0 | 164 | 0 |
| Lane Group Flow (vph) | 0 | 13 | 0 | 0 | 0 | 456 | 73 | 0 | 8 | 214 | 21 | 291 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 5\% | 0\% | 0\% | 6\% | 0\% | 0\% | 5\% | 6\% | 6\% |
| Turn Type | Perm | NA |  | Perm | Perm | NA | Perm | Perm | Perm | NA | Perm | pm+pt |
| Protected Phases |  | 4 |  |  |  | 4 |  |  |  | 2 |  | 1 |
| Permitted Phases | 4 |  |  | 4 | 4 |  | 4 | 2 | 2 |  | 2 | 6 |
| Actuated Green, G (s) |  | 36.1 |  |  |  | 36.1 | 36.1 |  | 11.1 | 11.1 | 11.1 | 34.2 |
| Effective Green, g (s) |  | 36.1 |  |  |  | 36.1 | 36.1 |  | 11.1 | 11.1 | 11.1 | 34.2 |
| Actuated g/C Ratio |  | 0.36 |  |  |  | 0.36 | 0.36 |  | 0.11 | 0.11 | 0.11 | 0.34 |
| Clearance Time (s) |  | 7.1 |  |  |  | 7.1 | 7.1 |  | 10.2 | 10.2 | 10.2 | 10.2 |
| Vehicle Extension (s) |  | 3.0 |  |  |  | 3.0 | 3.0 |  | 4.0 | 4.0 | 4.0 | 3.0 |
| Lane Grp Cap (vph) |  | 616 |  |  |  | 490 | 550 |  | 127 | 200 | 169 | 323 |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  | 0.12 |  | c0.12 |
| v/s Ratio Perm |  | 0.01 |  |  |  | c0.34 | 0.05 |  | 0.01 |  | 0.01 | c0.19 |
| v/c Ratio |  | 0.02 |  |  |  | 0.93 | 0.13 |  | 0.06 | 1.07 | 0.12 | 0.90 |
| Uniform Delay, d1 |  | 20.6 |  |  |  | 30.7 | 21.4 |  | 39.8 | 44.5 | 40.1 | 27.6 |
| Progression Factor |  | 1.00 |  |  |  | 0.89 | 1.02 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.0 |  |  |  | 3.5 | 0.0 |  | 1.0 | 83.4 | 1.5 | 26.6 |
| Delay (s) |  | 20.6 |  |  |  | 31.0 | 21.9 |  | 40.7 | 127.9 | 41.5 | 54.3 |
| Level of Service |  | C |  |  |  | C | C |  | D | F | D | D |
| Approach Delay (s) |  | 20.6 |  |  |  | 28.2 |  |  |  | 86.9 |  |  |
| Approach LOS |  | C |  |  |  | C |  |  |  | F |  |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 47.4 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.94 |  | 36.9 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $87.1 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave/R(a)rd)

|  | $\downarrow$ | \} | 4 |  | $\bigcirc$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR | NEL | NER | NER2 |
| Lane ${ }^{\text {\% }}$ \%onfigurations | $\uparrow$ |  | M |  | F |
| Traffic Volume (vph) | 208 | 11 | 2 | 11 | 21 |
| Future Volume (vph) | 208 | 11 | 2 | 11 | 21 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 10.2 |  | 9.4 |  | 9.4 |
| Lane Utill. Factor | 1.00 |  | 1.00 |  | 0.95 |
| Frt | 0.99 |  | 0.86 |  | 0.85 |
| Flt Protected | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (prot) | 1792 |  | 1615 |  | 1461 |
| Flt Permitted | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (perm) | 1792 |  | 1615 |  | 1461 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 236 | 12 | 2 | 12 | 24 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 18 |
| Lane Group Flow (vph) | 249 | 0 | 1 | 0 | 1 |
| Heavy Vehicles (\%) | 5\% | 9\% | 0\% | 0\% | 5\% |
| Turn Type | NA |  | Perm |  | Perm |
| Protected Phases | 6 |  |  |  |  |
| Permitted Phases |  |  | 3 |  | 3 |
| Actuated Green, G (s) | 34.2 |  | 3.0 |  | 3.0 |
| Effective Green, g (s) | 34.2 |  | 3.0 |  | 3.0 |
| Actuated g/C Ratio | 0.34 |  | 0.03 |  | 0.03 |
| Clearance Time (s) | 10.2 |  | 9.4 |  | 9.4 |
| Vehicle Extension (s) | 4.0 |  | 2.0 |  | 2.0 |
| Lane Grp Cap (vph) | 612 |  | 48 |  | 43 |
| v/s Ratio Prot | 0.14 |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  |  | 0.00 |  | c0.00 |
| v/c Ratio | 0.41 |  | 0.01 |  | 0.01 |
| Uniform Delay, d1 | 25.1 |  | 47.1 |  | 47.1 |
| Progression Factor | 1.00 |  | 1.00 |  | 1.00 |
| Incremental Delay, d2 | 2.0 |  | 0.0 |  | 0.0 |
| Delay (s) | 27.1 |  | 47.1 |  | 47.1 |
| Level of Service | C |  | D |  | D |
| Approach Delay (s) | 41.8 |  | 47.1 |  |  |
| Approach LOS | D |  | D |  |  |
| Intersection Summary |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)
09/16/2021

|  | 4 | $\rightarrow$ | 7 | 7 |  | 4 | 4 | $\dagger$ | 7 | ( | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | 4 | 「' |  | 4 |  |  |  |  |
| Traffic Volume (vph) | 203 | 285 | 0 | 0 | 544 | 413 | 175 | 0 | 238 | 0 | 0 | 0 |
| Future Volume (vph) | 203 | 285 | 0 | 0 | 544 | 413 | 175 | 0 | 238 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.1 |  |  | 6.1 | 6.1 |  | 5.3 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 1.00 | 0.85 |  | 0.92 |  |  |  |  |
| Flt Protected |  | 0.98 |  |  | 1.00 | 1.00 |  | 0.98 |  |  |  |  |
| Satd. Flow (prot) |  | 1763 |  |  | 1776 | 1538 |  | 1606 |  |  |  |  |
| Flt Permitted |  | 0.43 |  |  | 1.00 | 1.00 |  | 0.98 |  |  |  |  |
| Satd. Flow (perm) |  | 769 |  |  | 1776 | 1538 |  | 1606 |  |  |  |  |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 228 | 320 | 0 | 0 | 611 | 464 | 197 | 0 | 267 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 214 | 0 | 76 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 548 | 0 | 0 | 611 | 250 | 0 | 388 | 0 | 0 | 0 | 0 |
| Heavy Vehicles (\%) | 5\% | 6\% | 0\% | 0\% | 7\% | 5\% | 4\% | 0\% | 9\% | 0\% | 0\% | 0\% |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Perm | NA |  |  |  |  |
| Protected Phases | 1 | 6 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 6 |  |  |  |  | 2 | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 64.9 |  |  | 53.8 | 53.8 |  | 23.7 |  |  |  |  |
| Effective Green, g (s) |  | 64.9 |  |  | 53.8 | 53.8 |  | 23.7 |  |  |  |  |
| Actuated g/C Ratio |  | 0.65 |  |  | 0.54 | 0.54 |  | 0.24 |  |  |  |  |
| Clearance Time (s) |  | 6.1 |  |  | 6.1 | 6.1 |  | 5.3 |  |  |  |  |
| Vehicle Extension (s) |  | 5.0 |  |  | 5.0 | 5.0 |  | 5.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 548 |  |  | 955 | 827 |  | 380 |  |  |  |  |
| v/s Ratio Prot |  | c0.05 |  |  | 0.34 |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | c0.60 |  |  |  | 0.16 |  | 0.24 |  |  |  |  |
| v/c Ratio |  | 1.00 |  |  | 0.64 | 0.30 |  | 1.02 |  |  |  |  |
| Uniform Delay, d1 |  | 17.5 |  |  | 16.3 | 12.7 |  | 38.1 |  |  |  |  |
| Progression Factor |  | 0.67 |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  |  |
| Incremental Delay, d2 |  | 34.1 |  |  | 3.3 | 0.9 |  | 51.4 |  |  |  |  |
| Delay (s) |  | 45.8 |  |  | 19.6 | 13.7 |  | 89.6 |  |  |  |  |
| Level of Service |  | D |  |  | B | B |  | F |  |  |  |  |
| Approach Delay (s) |  | 45.8 |  |  | 17.0 |  |  | 89.6 |  |  | 0.0 |  |
| Approach LOS |  | D |  |  | B |  |  | F |  |  | A |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 40.7 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 1.06 |  | 17.5 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | F |
| Intersection Capacity Utilization | $93.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
4: Triangle Drive \& Route 256 (Weyers Cave Road)


HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave/Raqud)

|  | * |  |  | $\psi$ | $\cdots$ |  | 4 | $\cdots$ | 4 | $\dagger$ | $p$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL2 | WBL | WBT | WBR | NBL2 | NBL | NBT | NBR | SBL |
| Lane Configurations |  | \& |  |  |  | $\uparrow$ | 「 |  | ${ }^{*}$ | 4 | 「 | ${ }^{7}$ |
| Traffic Volume (vph) | 1 | 1 | 2 | 189 | 10 | 6 | 254 | 10 | 1 | 194 | 327 | 317 |
| Future Volume (vph) | 1 | 1 | 2 | 189 | 10 | 6 | 254 | 10 | 1 | 194 | 327 | 317 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 7.1 |  |  |  | 7.1 | 7.1 |  | 10.2 | 10.2 | 10.2 | 10.2 |
| Lane Util. Factor |  | 1.00 |  |  |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.93 |  |  |  | 1.00 | 0.85 |  | 1.00 | 1.00 | 0.85 | 1.00 |
| Fit Protected |  | 0.99 |  |  |  | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 |
| Satd. Flow (prot) |  | 1750 |  |  |  | 1779 | 1442 |  | 1805 | 1881 | 1583 | 1703 |
| Flt Permitted |  | 0.94 |  |  |  | 0.73 | 1.00 |  | 0.57 | 1.00 | 1.00 | 0.50 |
| Satd. Flow (perm) |  | 1665 |  |  |  | 1361 | 1442 |  | 1078 | 1881 | 1583 | 890 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 1 | 1 | 2 | 199 | 11 | 6 | 267 | 11 | 1 | 204 | 344 | 334 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 213 | 0 | 0 | 0 | 233 | 0 |
| Lane Group Flow (vph) | 0 | 4 | 0 | 0 | 0 | 216 | 54 | 0 | 12 | 204 | 111 | 334 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 0\% | 0\% | 12\% | 0\% | 0\% | 1\% | 2\% | 6\% |
| Turn Type | Perm | NA |  | Perm | Perm | NA | Perm | Perm | Perm | NA | Perm | pm+pt |
| Protected Phases |  | 4 |  |  |  | 4 |  |  |  | 2 |  | 1 |
| Permitted Phases | 4 |  |  | 4 | 4 |  | 4 | 2 | 2 |  | 2 | 6 |
| Actuated Green, G (s) |  | 24.1 |  |  |  | 24.1 | 24.1 |  | 38.8 | 38.8 | 38.8 | 66.2 |
| Effective Green, g (s) |  | 24.1 |  |  |  | 24.1 | 24.1 |  | 38.8 | 38.8 | 38.8 | 66.2 |
| Actuated g/C Ratio |  | 0.20 |  |  |  | 0.20 | 0.20 |  | 0.32 | 0.32 | 0.32 | 0.55 |
| Clearance Time (s) |  | 7.1 |  |  |  | 7.1 | 7.1 |  | 10.2 | 10.2 | 10.2 | 10.2 |
| Vehicle Extension (s) |  | 3.0 |  |  |  | 3.0 | 3.0 |  | 4.0 | 4.0 | 4.0 | 3.0 |
| Lane Grp Cap (vph) |  | 334 |  |  |  | 273 | 289 |  | 348 | 608 | 511 | 607 |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  | 0.11 |  | c0.08 |
| v/s Ratio Perm |  | 0.00 |  |  |  | c0.16 | 0.04 |  | 0.01 |  | 0.07 | c0.22 |
| v/c Ratio |  | 0.01 |  |  |  | 0.79 | 0.19 |  | 0.03 | 0.34 | 0.22 | 0.55 |
| Uniform Delay, d1 |  | 38.4 |  |  |  | 45.6 | 39.8 |  | 27.8 | 30.8 | 29.6 | 15.6 |
| Progression Factor |  | 1.00 |  |  |  | 0.96 | 0.89 |  | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.0 |  |  |  | 1.5 | 0.0 |  | 0.2 | 1.5 | 1.0 | 1.1 |
| Delay (s) |  | 38.4 |  |  |  | 45.2 | 35.7 |  | 28.0 | 32.3 | 30.5 | 16.7 |
| Level of Service |  | D |  |  |  | D | D |  | C | C | C | B |
| Approach Delay (s) |  | 38.4 |  |  |  | 39.9 |  |  |  | 31.1 |  |  |
| Approach LOS |  | D |  |  |  | D |  |  |  | C |  |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 28.3 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.64 |  | 36.9 |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | D |
| Intersection Capacity Utilization | $80.7 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

HCM Signalized Intersection Capacity Analysis
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers CaN\&/R(Berd)


HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp


HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)
09/16/2021

|  | 4 | $\rightarrow$ | 7 | 7 |  | 4 | 4 | $\dagger$ | $p$ | ( | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | 4 | 「' |  | * |  |  |  |  |
| Traffic Volume (vph) | 183 | 667 | 0 | 0 | 397 | 288 | 114 | 0 | 255 | 0 | 0 | 0 |
| Future Volume (vph) | 183 | 667 | 0 | 0 | 397 | 288 | 114 | 0 | 255 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.1 |  |  | 6.1 | 6.1 |  | 5.3 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 1.00 | 0.85 |  | 0.91 |  |  |  |  |
| Flt Protected |  | 0.99 |  |  | 1.00 | 1.00 |  | 0.98 |  |  |  |  |
| Satd. Flow (prot) |  | 1792 |  |  | 1776 | 1553 |  | 1622 |  |  |  |  |
| Flt Permitted |  | 0.72 |  |  | 1.00 | 1.00 |  | 0.98 |  |  |  |  |
| Satd. Flow (perm) |  | 1296 |  |  | 1776 | 1553 |  | 1622 |  |  |  |  |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 197 | 717 | 0 | 0 | 427 | 310 | 123 | 0 | 274 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 122 | 0 | 67 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 914 | 0 | 0 | 427 | 188 | 0 | 330 | 0 | 0 | 0 | 0 |
| Heavy Vehicles (\%) | 1\% | 6\% | 0\% | 0\% | 7\% | 4\% | 6\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Turn Type | pm+pt | NA |  |  | NA | Perm | Perm | NA |  |  |  |  |
| Protected Phases | 1 | 6 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 6 |  |  |  |  | 2 | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 83.9 |  |  | 72.8 | 72.8 |  | 24.7 |  |  |  |  |
| Effective Green, g (s) |  | 83.9 |  |  | 72.8 | 72.8 |  | 24.7 |  |  |  |  |
| Actuated g/C Ratio |  | 0.70 |  |  | 0.61 | 0.61 |  | 0.21 |  |  |  |  |
| Clearance Time (s) |  | 6.1 |  |  | 6.1 | 6.1 |  | 5.3 |  |  |  |  |
| Vehicle Extension (s) |  | 5.0 |  |  | 5.0 | 5.0 |  | 5.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 926 |  |  | 1077 | 942 |  | 333 |  |  |  |  |
| v/s Ratio Prot |  | c0.04 |  |  | 0.24 |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | c0.65 |  |  |  | 0.12 |  | 0.20 |  |  |  |  |
| v/c Ratio |  | 0.99 |  |  | 0.40 | 0.20 |  | 0.99 |  |  |  |  |
| Uniform Delay, d1 |  | 17.5 |  |  | 12.2 | 10.6 |  | 47.5 |  |  |  |  |
| Progression Factor |  | 0.69 |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  |  |
| Incremental Delay, d2 |  | 19.5 |  |  | 1.1 | 0.5 |  | 47.1 |  |  |  |  |
| Delay (s) |  | 31.6 |  |  | 13.3 | 11.0 |  | 94.6 |  |  |  |  |
| Level of Service |  | C |  |  | B | B |  | F |  |  |  |  |
| Approach Delay (s) |  | 31.6 |  |  | 12.4 |  |  | 94.6 |  |  | 0.0 |  |
| Approach LOS |  | C |  |  | B |  |  | F |  |  | A |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 36.9 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 1.04 |  | 17.5 |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | G |
| Intersection Capacity Utilization | $102.7 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
4: Triangle Drive \& Route 256 (Weyers Cave Road)


Queues
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cane/ZR(zad)

|  | $\rightarrow$ |  | 4 | , | $\dagger$ | $p$ | * | $\downarrow$ | 4 | $\neg$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT | NEL | NER2 |
| Lane Group Flow (vph) | 13 | 456 | 203 | 8 | 214 | 185 | 291 | 249 | 20 | 19 |
| v/c Ratio | 0.02 | 0.93 | 0.28 | 0.05 | 0.80 | 0.41 | 0.85 | 0.37 | 0.06 | 0.06 |
| Control Delay | 21.8 | 33.9 | 0.5 | 39.0 | 65.0 | 4.1 | 51.8 | 25.7 | 0.3 | 0.4 |
| Queue Delay | 0.0 | 6.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 21.8 | 40.2 | 0.5 | 39.0 | 65.0 | 4.1 | 51.8 | 25.7 | 0.3 | 0.4 |
| Queue Length 50th (ft) | 5 | 262 | 0 | 5 | 136 | 0 | 147 | 121 | 0 | 0 |
| Queue Length 95th (ft) | 18 | m241 | m0 | 18 | \#261 | 13 | \#265 | 186 | 0 | 0 |
| Internal Link Dist (tt) | 467 | 317 |  |  | 841 |  |  | 1001 | 128 |  |
| Turn Bay Length (ft) |  |  | 200 | 130 |  | 130 | 350 |  |  |  |
| Base Capacity (vph) | 616 | 489 | 736 | 170 | 268 | 446 | 342 | 680 | 334 | 326 |
| Starvation Cap Reductn | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.02 | 0.97 | 0.28 | 0.05 | 0.80 | 0.41 | 0.85 | 0.37 | 0.06 | 0.06 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th per | queue | metere | by upstr | m sign |  |  |  |  |  |  |

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp

| Lane Group | EBT | EBR | WBT | SBT |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 341 | 153 | 817 | 470 |
| v/c Ratio | 0.36 | 0.17 | 1.06 | 1.03 |
| Control Delay | 5.8 | 0.3 | 58.2 | 80.0 |
| Queue Delay | 0.6 | 0.0 | 0.0 | 26.5 |
| Total Delay | 6.4 | 0.3 | 58.2 | 106.5 |
| Queue Length 50th ( ft ) | 45 | 1 | ~155 | $\sim 251$ |
| Queue Length 95th (ft) | m52 | m0 | m\#675 | \#431 |
| Internal Link Dist (ft) | 317 |  | 737 | 874 |
| Turn Bay Length (ft) |  | 250 |  |  |
| Base Capacity (vph) | 955 | 884 | 770 | 455 |
| Starvation Cap Reductn | 295 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 119 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.52 | 0.17 | 1.06 | 1.40 |
| Intersection Summary |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longe |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signa |  |  |  |  |


|  | $\rightarrow$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBT |
| Lane Group Flow (vph) | 548 | 611 | 464 | 464 |
| v/c Ratio | 1.00 | 0.64 | 0.45 | 1.02 |
| Control Delay | 50.7 | 20.1 | 2.6 | 77.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 50.7 | 20.1 | 2.6 | 77.8 |
| Queue Length 50th (ft) | ~96 | 260 | 0 | $\sim 252$ |
| Queue Length 95th (ft) | m\#252 | 372 | 43 | \#451 |
| Internal Link Dist (ft) | 737 | 805 |  | 951 |
| Turn Bay Length (ft) |  |  |  |  |
| Base Capacity (vph) | 548 | 955 | 1041 | 456 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.00 | 0.64 | 0.45 | 1.02 |
| Intersection Summary |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longe |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signa |  |  |  |  |

Queues
1: Gas Station \& US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cane/ZR(zad)

|  | $\rightarrow$ | $\bullet$ | 4 | 4 | $\dagger$ | 7 | - | 1 | 4 | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT | NEL | NER2 |
| Lane Group Flow (vph) | 4 | 216 | 267 | 12 | 204 | 344 | 334 | 318 | 15 | 10 |
| v/c Ratio | 0.01 | 0.79 | 0.53 | 0.03 | 0.31 | 0.44 | 0.53 | 0.30 | 0.05 | 0.04 |
| Control Delay | 35.2 | 45.4 | 4.5 | 35.5 | 34.9 | 6.0 | 18.8 | 16.0 | 0.4 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.2 | 45.4 | 4.6 | 35.5 | 34.9 | 6.0 | 18.8 | 16.0 | 0.4 | 0.2 |
| Queue Length 50th (ft) | 2 | 152 | 0 | 7 | 129 | 0 | 149 | 138 | 0 | 0 |
| Queue Length 95th (ft) | 12 | m135 | m0 | 24 | 215 | 78 | 231 | 214 | 0 | 0 |
| Internal Link Dist (ft) | 467 | 317 |  |  | 841 |  |  | 1001 | 128 |  |
| Turn Bay Length (ft) |  |  | 200 | 130 |  | 130 | 350 |  |  |  |
| Base Capacity (vph) | 400 | 328 | 549 | 382 | 667 | 783 | 666 | 1063 | 279 | 277 |
| Starvation Cap Reductn | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.01 | 0.66 | 0.52 | 0.03 | 0.31 | 0.44 | 0.50 | 0.30 | 0.05 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp

|  | $\rightarrow$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBT | SBT |
| Lane Group Flow (vph) | 508 | 196 | 549 | 609 |
| v/c Ratio | 0.56 | 0.24 | 1.05 | 1.07 |
| Control Delay | 16.1 | 1.0 | 74.2 | 90.9 |
| Queue Delay | 0.5 | 0.0 | 0.0 | 0.0 |
| Total Delay | 16.5 | 1.0 | 74.2 | 90.9 |
| Queue Length 50th (ft) | 145 | 0 | $\sim 275$ | $\sim 458$ |
| Queue Length 95th (ft) | 152 | 5 | m\#476 | \#686 |
| Internal Link Dist (ft) | 317 |  | 742 | 874 |
| Turn Bay Length (ft) |  | 250 |  |  |
| Base Capacity (vph) | 904 | 832 | 523 | 570 |
| Starvation Cap Reductn | 113 | 0 | 0 | 0 |
| Spillback Cap Reductn | 10 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.64 | 0.24 | 1.05 | 1.07 |
| Intersection Summary |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longe |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signa |  |  |  |  |


|  | $\rightarrow$ |  | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBT |
| Lane Group Flow (vph) | 914 | 427 | 310 | 397 |
| v/c Ratio | 0.99 | 0.40 | 0.29 | 0.99 |
| Control Delay | 34.1 | 13.6 | 1.8 | 81.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 13.6 | 1.8 | 81.2 |
| Queue Length 50th (tt) | 253 | 161 | 0 | 253 |
| Queue Length 95th (tt) | m\#371 | 229 | 35 | 461 |
| Internal Link Dist (ft) | 742 | 798 |  | 951 |
| Turn Bay Length (tt) |  |  |  |  |
| Base Capacity (vph) | 927 | 1077 | 1064 | 400 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.99 | 0.40 | 0.29 | 0.99 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer |  |  |  |  |
|  |  |  |  |  |
| m Volume for 95th per | queue | metere | by ups | n sig |

4. Appendix D: Synchro Report - Future Build Conditions

HCM Signalized Intersection Capacity Analysis
1: US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave Road)

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 | ${ }^{7}$ | 4 | F | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 4 | 16 | 4 | 401 | 0 | 179 | , | 188 | 174 | 256 | 219 | 0 |
| Future Volume (vph) | 4 | 16 | 4 | 401 | 0 | 179 | 1 | 188 | 174 | 256 | 219 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 7.1 |  |  | 7.1 | 7.1 | 7.7 | 7.7 | 7.7 | 9.1 | 9.1 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt |  | 0.98 |  |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  |
| Flt Protected |  | 0.99 |  |  | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1838 |  |  | 1770 | 1524 | 1805 | 1810 | 1524 | 1703 | 1810 |  |
| Flt Permitted |  | 0.92 |  |  | 0.74 | 1.00 | 0.60 | 1.00 | 1.00 | 0.36 | 1.00 |  |
| Satd. Flow (perm) |  | 1713 |  |  | 1377 | 1524 | 1149 | 1810 | 1524 | 645 | 1810 |  |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 5 | 18 | 5 | 456 | 0 | 203 | 1 | 214 | 198 | 291 | 249 | 0 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 0 | 127 | 0 | 0 | 158 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 25 | 0 | 0 | 456 | 76 | 1 | 214 | 40 | 291 | 249 | 0 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 0\% | 6\% | 0\% | 5\% | 6\% | 6\% | 5\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 4 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 4 |  | 4 | 2 |  | 2 | 6 |  |  |
| Actuated Green, G (s) |  | 29.9 |  |  | 29.9 | 29.9 | 17.0 | 16.0 | 16.0 | 33.9 | 25.2 |  |
| Effective Green, g (s) |  | 29.9 |  |  | 29.9 | 29.9 | 17.0 | 16.0 | 16.0 | 33.9 | 25.2 |  |
| Actuated g/C Ratio |  | 0.37 |  |  | 0.37 | 0.37 | 0.21 | 0.20 | 0.20 | 0.42 | 0.31 |  |
| Clearance Time (s) |  | 7.1 |  |  | 7.1 | 7.1 | 7.7 | 7.7 | 7.7 | 9.1 | 9.1 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 |  |
| Lane Grp Cap (vph) |  | 640 |  |  | 514 | 569 | 252 | 362 | 304 | 408 | 570 |  |
| v/s Ratio Prot |  |  |  |  |  |  | 0.00 | 0.12 |  | c0.09 | 0.14 |  |
| v/s Ratio Perm |  | 0.01 |  |  | c0.33 | 0.05 | 0.00 |  | 0.03 | c0.21 |  |  |
| v/c Ratio |  | 0.04 |  |  | 0.89 | 0.13 | 0.00 | 0.59 | 0.13 | 0.71 | 0.44 |  |
| Uniform Delay, d1 |  | 15.9 |  |  | 23.5 | 16.5 | 24.8 | 29.0 | 26.3 | 16.9 | 21.8 |  |
| Progression Factor |  | 1.00 |  |  | 1.11 | 1.38 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.0 |  |  | 14.6 | 0.1 | 0.0 | 6.9 | 0.9 | 5.8 | 2.4 |  |
| Delay (s) |  | 15.9 |  |  | 40.6 | 22.9 | 24.8 | 36.0 | 27.2 | 22.7 | 24.2 |  |
| Level of Service |  | B |  |  | D | C | C | D | C | C | C |  |
| Approach Delay (s) |  | 15.9 |  |  | 35.1 |  |  | 31.7 |  |  | 23.4 |  |
| Approach LOS |  | B |  |  | D |  |  | C |  |  | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 30.1 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.85 |  | 23.9 |
| Actuated Cycle Length (s) | 80.0 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $72.9 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

Analysis Period (min)
15
c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp
04/19/2022


HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)


Queues
1: US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave Road)

|  | $\rightarrow$ |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Group Flow (vph) | 28 | 456 | 203 | 1 | 214 | 198 | 291 | 249 |
| v/c Ratio | 0.04 | 0.89 | 0.29 | 0.00 | 0.59 | 0.43 | 0.72 | 0.35 |
| Control Delay | 13.2 | 43.9 | 4.6 | 15.0 | 38.1 | 7.9 | 30.5 | 21.4 |
| Queue Delay | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 13.2 | 44.2 | 4.6 | 15.0 | 38.1 | 7.9 | 30.5 | 21.4 |
| Queue Length 50th (ft) | 7 | 240 | 7 | 0 | 101 | 0 | 103 | 84 |
| Queue Length 95th (ft) | 22 | m\#349 | m24 | 3 | \#172 | 51 | \#168 | 178 |
| Internal Link Dist (ft) | 467 | 317 |  |  | 841 |  |  | 1001 |
| Turn Bay Length (ft) |  |  | 200 | 130 |  | 130 | 350 |  |
| Base Capacity (vph) | 686 | 549 | 729 | 347 | 361 | 463 | 402 | 708 |
| Starvation Cap Reductn | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.04 | 0.84 | 0.28 | 0.00 | 0.59 | 0.43 | 0.72 | 0.35 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| m Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp

|  | $\rightarrow$ | 7 | 7 |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBL | WBT | SBT |
| Lane Group Flow (vph) | 341 | 153 | 414 | 403 | 470 |
| v/c Ratio | 0.62 | 0.27 | 0.67 | 0.38 | 0.87 |
| Control Delay | 18.5 | 2.5 | 8.3 | 3.0 | 35.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.1 | 0.5 |
| Total Delay | 18.5 | 2.5 | 8.3 | 3.0 | 36.2 |
| Queue Length 50th ( ft ) | 153 | 11 | 43 | 40 | 142 |
| Queue Length 95th (ft) | m164 | m15 | m50 | m46 | \#287 |
| Internal Link Dist (ft) | 317 |  |  | 737 | 874 |
| Turn Bay Length (ft) |  | 250 | 225 |  |  |
| Base Capacity (vph) | 551 | 575 | 619 | 1059 | 581 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 75 | 12 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.62 | 0.27 | 0.67 | 0.41 | 0.83 |
| Intersection Summary |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
|  |  |  |  |  |  |
| m Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |


|  | $\rangle$ |  | 4 | 4 | $\uparrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | NBT |
| Lane Group Flow (vph) | 228 | 320 | 611 | 464 | 464 |
| v/c Ratio | 0.61 | 0.30 | 0.77 | 0.49 | 0.91 |
| Control Delay | 12.9 | 2.9 | 27.4 | 3.5 | 44.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 12.9 | 2.9 | 27.4 | 3.5 | 44.7 |
| Queue Length 50th (ft) | 21 | 32 | 253 | 0 | 166 |
| Queue Length 95th (ft) | m49 | m36 | \#395 | 49 | \#334 |
| Internal Link Dist (ft) |  | 737 | 805 |  | 951 |
| Turn Bay Length (ft) | 215 |  |  |  |  |
| Base Capacity (vph) | 373 | 1067 | 791 | 942 | 526 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.61 | 0.30 | 0.77 | 0.49 | 0.88 |
| Intersection Summary |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |
| m Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |

Queues
1: US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave Road)

|  | $\rightarrow$ |  |  | 4 | $\dagger$ | $>$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Group Flow (vph) | 19 | 215 | 267 | 1 | 204 | 344 | 334 | 318 |
| v/c Ratio | 0.05 | 0.75 | 0.51 | 0.00 | 0.38 | 0.49 | 0.57 | 0.31 |
| Control Delay | 21.8 | 46.9 | 10.5 | 24.0 | 27.4 | 5.9 | 14.3 | 10.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.0 |
| Total Delay | 21.8 | 46.9 | 10.5 | 24.0 | 27.4 | 6.0 | 14.4 | 10.7 |
| Queue Length 50th (ft) | 6 | 106 | 27 | 0 | 88 | 0 | 90 | 83 |
| Queue Length 95th (ft) | 23 | m146 | m57 | 4 | 151 | 64 | 146 | 135 |
| Internal Link Dist (ft) | 467 | 317 |  |  | 841 |  |  | 1001 |
| Turn Bay Length (ft) |  |  | 200 | 130 |  | 130 | 350 |  |
| Base Capacity (vph) | 412 | 332 | 559 | 308 | 537 | 698 | 603 | 1038 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 29 | 22 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.65 | 0.48 | 0.00 | 0.38 | 0.51 | 0.57 | 0.31 |
| Intersection Summary |  |  |  |  |  |  |  |  |
| m Volume for 95th perc | queue | metere | by upst | am sign |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
1: US Route 11 (Lee Highway) \& Ridgetop Drive/Route 256 (Weyers Cave Road)

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ | F゙ | ${ }^{*}$ | 4 | 「 | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 6 | 10 | 2 | 199 | 6 | 254 | 1 | 194 | 327 | 317 | 301 | 1 |
| Future Volume (vph) | 6 | 10 | 2 | 199 | 6 | 254 | 1 | 194 | 327 | 317 | 301 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 7.1 |  |  | 7.1 | 7.1 | 10.2 | 10.2 | 10.2 | 10.2 | 10.2 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt |  | 0.99 |  |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  |
| Flt Protected |  | 0.98 |  |  | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1844 |  |  | 1777 | 1442 | 1805 | 1881 | 1583 | 1703 | 1826 |  |
| Flt Permitted |  | 0.88 |  |  | 0.72 | 1.00 | 0.57 | 1.00 | 1.00 | 0.44 | 1.00 |  |
| Satd. Flow (perm) |  | 1654 |  |  | 1339 | 1442 | 1078 | 1881 | 1583 | 781 | 1826 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 6 | 11 | 2 | 209 | 6 | 267 | 1 | 204 | 344 | 334 | 317 | 1 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 210 | 0 | 0 | 246 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 17 | 0 | 0 | 215 | 57 | 1 | 204 | 98 | 334 | 318 | 0 |
| Heavy Vehicles (\%) | 0\% | 0\% | 0\% | 2\% | 0\% | 12\% | 0\% | 1\% | 2\% | 6\% | 4\% | 0\% |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 4 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 4 |  | 4 | 2 |  | 2 | 6 |  |  |
| Actuated Green, G (s) |  | 17.2 |  |  | 17.2 | 17.2 | 22.9 | 22.9 | 22.9 | 45.5 | 45.5 |  |
| Effective Green, g (s) |  | 17.2 |  |  | 17.2 | 17.2 | 22.9 | 22.9 | 22.9 | 45.5 | 45.5 |  |
| Actuated g/C Ratio |  | 0.21 |  |  | 0.21 | 0.21 | 0.29 | 0.29 | 0.29 | 0.57 | 0.57 |  |
| Clearance Time (s) |  | 7.1 |  |  | 7.1 | 7.1 | 10.2 | 10.2 | 10.2 | 10.2 | 10.2 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 | 3.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 |  |
| Lane Grp Cap (vph) |  | 355 |  |  | 287 | 310 | 308 | 538 | 453 | 587 | 1038 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  | 0.11 |  | c0.09 | 0.17 |  |
| v/s Ratio Perm |  | 0.01 |  |  | c0.16 | 0.04 | 0.00 |  | 0.06 | c0.24 |  |  |
| v/c Ratio |  | 0.05 |  |  | 0.75 | 0.19 | 0.00 | 0.38 | 0.22 | 0.57 | 0.31 |  |
| Uniform Delay, d1 |  | 24.9 |  |  | 29.4 | 25.7 | 20.4 | 22.9 | 21.7 | 10.2 | 9.0 |  |
| Progression Factor |  | 1.00 |  |  | 1.14 | 2.01 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.1 |  |  | 8.6 | 0.2 | 0.0 | 2.0 | 1.1 | 1.3 | 0.8 |  |
| Delay (s) |  | 25.0 |  |  | 42.0 | 51.8 | 20.4 | 24.9 | 22.8 | 11.4 | 9.8 |  |
| Level of Service |  | C |  |  | D | D | C | C | C | B | A |  |
| Approach Delay (s) |  | 25.0 |  |  | 47.4 |  |  | 23.6 |  |  | 10.6 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 25.4 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.69 |  | 27.5 |
| Actuated Cycle Length (s) | 80.0 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $69.1 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |

Analysis Period (min)
15
C Critical Lane Group

Queues
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp

|  | $\rightarrow$ | \% |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBL | WBT | SBT |
| Lane Group Flow (vph) | 508 | 196 | 259 | 290 | 609 |
| v/c Ratio | 0.80 | 0.30 | 0.72 | 0.31 | 0.95 |
| Control Delay | 28.3 | 1.9 | 19.9 | 3.6 | 47.0 |
| Queue Delay | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.5 | 1.9 | 19.9 | 3.6 | 47.0 |
| Queue Length 50th (ft) | 228 | 1 | 33 | 28 | 224 |
| Queue Length 95th (ft) | \#370 | 7 | m\#109 | m37 | \#438 |
| Internal Link Dist (ft) | 317 |  |  | 742 | 874 |
| Turn Bay Length (ft) |  | 250 | 225 |  |  |
| Base Capacity (vph) | 638 | 645 | 361 | 934 | 645 |
| Starvation Cap Reductn | 8 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.81 | 0.30 | 0.72 | 0.31 | 0.94 |
| Intersection Summary |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |
| $m$ Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Route 256 (Weyers Cave Road) \& I-81 Southbound Ramp
04/19/2022


Queues
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)

|  | $\dagger$ |  | 4 | 4 | $\uparrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | NBT |
| Lane Group Flow (vph) | 197 | 717 | 427 | 310 | 397 |
| v/c Ratio | 0.35 | 0.65 | 0.52 | 0.35 | 0.80 |
| Control Delay | 3.4 | 4.5 | 19.1 | 3.2 | 29.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 3.4 | 4.5 | 19.1 | 3.2 | 29.8 |
| Queue Length 50th (ft) | 13 | 81 | 148 | 0 | 118 |
| Queue Length 95th (ft) | m22 | m145 | 252 | 45 | 210 |
| Internal Link Dist (ft) |  | 742 | 798 |  | 951 |
| Turn Bay Length (ft) | 215 |  |  |  |  |
| Base Capacity (vph) | 569 | 1103 | 827 | 889 | 580 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.35 | 0.65 | 0.52 | 0.35 | 0.68 |
| Intersection Summary |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
3: I-81 Northbound Ramp \& Route 256 (Weyers Cave Road)

5. Appendix E: SIDRA Report - Future Build Conditions

## SITE LAYOUT

$\theta$ Site: 101 [US 11 - AM (No Reroute)]
New Site
Site Category: (None)
Roundabout


SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MICHAEL BAKER INTERNATIONAL | Created: Thursday, April 21, 2022 12:32:39 PM
Project: \IIRICHFS1.bkr.mbakercorp.comIPROJECTSISAWMPOIWork_Files\Analysis\Build\Build_Alts_VDOT\Pref_Alt_Roundabouts.sip8

## MOVEMENT SUMMARY

## Site: 101 [US 11 - AM (No Reroute)]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: US 11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3u | U | 7 | 0.0 | 0.447 | 9.1 | LOS A | 3.2 | 83.0 | 0.67 | 0.54 | 0.67 | 34.4 |
| 3 | L2 | 1 | 0.0 | 0.447 | 9.1 | LOS A | 3.2 | 83.0 | 0.67 | 0.54 | 0.67 | 23.3 |
| 8 | T1 | 214 | 5.0 | 0.447 | 9.3 | LOS A | 3.2 | 83.0 | 0.67 | 0.54 | 0.67 | 33.3 |
| 18 | R2 | 185 | 6.0 | 0.447 | 9.4 | LOS A | 3.2 | 83.0 | 0.67 | 0.54 | 0.67 | 21.1 |
| Appr |  | 407 | 5.4 | 0.447 | 9.3 | LOS A | 3.2 | 83.0 | 0.67 | 0.54 | 0.67 | 27.9 |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 456 | 2.0 | 0.641 | 12.7 | LOS B | 7.5 | 192.2 | 0.71 | 0.60 | 0.84 | 26.4 |
| 6 | T1 | 1 | 0.0 | 0.641 | 12.6 | LOS B | 7.5 | 192.2 | 0.71 | 0.60 | 0.84 | 11.6 |
| 16 | R2 | 203 | 6.0 | 0.641 | 12.8 | LOS B | 7.5 | 192.2 | 0.71 | 0.60 | 0.84 | 25.2 |
| Appro |  | 660 | 3.2 | 0.641 | 12.7 | LOS B | 7.5 | 192.2 | 0.71 | 0.60 | 0.84 | 26.0 |
| North: US 11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 291 | 6.0 | 0.672 | 16.5 | LOS B | 9.0 | 235.0 | 0.88 | 1.02 | 1.37 | 20.4 |
| 4 | T1 | 249 | 5.0 | 0.672 | 16.5 | LOS B | 9.0 | 235.0 | 0.88 | 1.02 | 1.37 | 29.1 |
| 14 | R2 | 1 | 0.0 | 0.672 | 16.2 | LOS B | 9.0 | 235.0 | 0.88 | 1.02 | 1.37 | 20.4 |
| Approach |  | 541 | 5.5 | 0.672 | 16.5 | LOS B | 9.0 | 235.0 | 0.88 | 1.02 | 1.37 | 24.7 |
| West: Ridegetop Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 5 | 0.0 | 0.056 | 8.2 | LOS A | 0.4 | 9.0 | 0.86 | 0.71 | 0.86 | 31.2 |
| 2 | T1 | 18 | 0.0 | 0.056 | 8.2 | LOS A | 0.4 | 9.0 | 0.86 | 0.71 | 0.86 | 9.5 |
| 12 | R2 | 5 | 0.0 | 0.056 | 8.2 | LOS A | 0.4 | 9.0 | 0.86 | 0.71 | 0.86 | 29.4 |
| Appro |  | 27 | 0.0 | 0.056 | 8.2 | LOS A | 0.4 | 9.0 | 0.86 | 0.71 | 0.86 | 16.4 |
| All Ve | cles | 1635 | 4.5 | 0.672 | 13.1 | LOS B | 9.0 | 235.0 | 0.76 | 0.73 | 0.97 | 25.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MICHAEL BAKER INTERNATIONAL | Processed: Thursday, April 21, 2022 12:31:45 PM
Project: $\ \backslash$ RICHFS1.bkr.mbakercorp.com\PROJECTSISAWMPOIWork_Files\Analysis\Build\Build_Alts_VDOT\Pref_Alt_Roundabouts.sip8

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
$\theta$ Site: 101 [US 11 - AM (No Reroute)]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| Vehicle Queue (\%ile) | 83 | 192 | 235 | 9 | 235 |



Colour code based on Queue Storage Ratio

| $\square[<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ | $\square 0.8-0.9]$ | $\square 0.9-1.0]$ |
| :---: | :---: | :---: | :---: | :---: |
| $[>1.0]$ |  |  |  |  |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\theta$ Site: 101 [US 11 - AM (No Reroute)]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| Delay (Control) | 9.3 | 12.7 | 16.5 | 8.2 | 13.1 |
| LOS | A | B | B | A | B |



Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## SITE LAYOUT

$\theta$ Site: 101 [US 11 - PM (No Reroute)]
New Site
Site Category: (None)
Roundabout


## MOVEMENT SUMMARY

## Site: 101 [US 11 - PM (No Reroute)]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Demand Total veh/h | $\begin{gathered} =10 w s \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: US 11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 u | U | 11 | 0.0 | 0.600 | 12.4 | LOS B | 6.7 | 169.7 | 0.77 | 0.76 | 1.00 | 32.8 |
| 3 | L2 | 1 | 0.0 | 0.600 | 12.4 | LOS B | 6.7 | 169.7 | 0.77 | 0.76 | 1.00 | 22.0 |
| 8 | T1 | 204 | 1.0 | 0.600 | 12.5 | LOS B | 6.7 | 169.7 | 0.77 | 0.76 | 1.00 | 31.8 |
| 18 | R2 | 344 | 2.0 | 0.600 | 12.5 | LOS B | 6.7 | 169.7 | 0.77 | 0.76 | 1.00 | 20.1 |
| Appr |  | 560 | 1.6 | 0.600 | 12.5 | LOS B | 6.7 | 169.7 | 0.77 | 0.76 | 1.00 | 24.7 |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 209 | 2.0 | 0.490 | 9.3 | LOS A | 3.7 | 98.4 | 0.60 | 0.44 | 0.60 | 28.8 |
| 6 | T1 | 6 | 0.0 | 0.490 | 9.3 | LOS A | 3.7 | 98.4 | 0.60 | 0.44 | 0.60 | 12.6 |
| 16 | R2 | 267 | 12.0 | 0.490 | 9.7 | LOS A | 3.7 | 98.4 | 0.60 | 0.44 | 0.60 | 27.1 |
| Appr |  | 483 | 7.5 | 0.490 | 9.6 | LOS A | 3.7 | 98.4 | 0.60 | 0.44 | 0.60 | 27.7 |
| North: US 11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 334 | 6.0 | 0.640 | 12.8 | LOS B | 7.4 | 191.2 | 0.70 | 0.59 | 0.82 | 21.6 |
| 4 | T1 | 317 | 4.0 | 0.640 | 12.8 | LOS B | 7.4 | 191.2 | 0.70 | 0.59 | 0.82 | 30.6 |
| 14 | R2 | 1 | 0.0 | 0.640 | 12.6 | LOS B | 7.4 | 191.2 | 0.70 | 0.59 | 0.82 | 21.6 |
| Approach |  | 652 | 5.0 | 0.640 | 12.8 | LOS B | 7.4 | 191.2 | 0.70 | 0.59 | 0.82 | 26.3 |
| West: Ridgetop Drive |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 6 | 0.0 | 0.034 | 6.8 | LOS A | 0.2 | 5.2 | 0.80 | 0.61 | 0.80 | 31.5 |
| 2 | T1 | 11 | 0.0 | 0.034 | 6.8 | LOS A | 0.2 | 5.2 | 0.80 | 0.61 | 0.80 | 9.9 |
| 12 | R2 | 2 | 0.0 | 0.034 | 6.8 | LOS A | 0.2 | 5.2 | 0.80 | 0.61 | 0.80 | 29.7 |
| Appr |  | 19 | 0.0 | 0.034 | 6.8 | LOS A | 0.2 | 5.2 | 0.80 | 0.61 | 0.80 | 19.2 |
| All Ve | icles | 1714 | 4.5 | 0.640 | 11.7 | LOS B | 7.4 | 191.2 | 0.70 | 0.60 | 0.82 | 26.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MICHAEL BAKER INTERNATIONAL | Processed: Thursday, April 21, 2022 12:31:44 PM
Project: $\ \backslash R I C H F S 1 . b k r$.mbakercorp.com\PROJECTSISAWMPOIWork_Files\Analysis\Build\Build_Alts_VDOT\Pref_Alt_Roundabouts.sip8

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
$\theta$ Site: 101 [US 11 - PM (No Reroute)]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| Vehicle Queue (\%ile) | 170 | 98 | 191 | 5 | 191 |



Colour code based on Queue Storage Ratio

| $\square<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ |
| :---: | :---: | :---: |
| $[0.8-0.9]$ | $\square 0.9-1.0]$ | $[>1.0]$ |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\square$ Site: 101 [US 11 - PM (No Reroute)]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| Delay (Control) | 12.5 | 9.6 | 12.8 | 6.8 | 11.7 |
| LOS | B | A | B | A | B |



Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## SITE LAYOUT

(7) Site: 101 [I81 SB TERMINII - AM]

New Site
Site Category: (None)
Roundabout


## MOVEMENT SUMMARY

## Site: 101 [I81 SB TERMINII - AM]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} =10 w s \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 414 | 9.0 | 0.640 | 10.9 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 36.1 |
| 6 | T1 | 403 | 4.0 | 0.640 | 10.8 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 26.8 |
| Appr |  | 817 | 6.5 | 0.640 | 10.9 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 32.6 |
| North: 181 NB Off-ramp |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 214 | 10.0 | 0.715 | 21.8 | LOS C | 8.7 | 228.6 | 0.94 | 1.22 | 1.68 | 24.1 |
| 4 | T1 | 1 | 0.0 | 0.715 | 21.1 | LOS C | 8.7 | 228.6 | 0.94 | 1.22 | 1.68 | 27.5 |
| 14 | R2 | 256 | 4.0 | 0.715 | 21.4 | LOS C | 8.7 | 228.6 | 0.94 | 1.22 | 1.68 | 21.4 |
| Approach |  | 470 | 6.7 | 0.715 | 21.6 | LOS C | 8.7 | 228.6 | 0.94 | 1.22 | 1.68 | 22.6 |
| West: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 341 | 5.0 | 0.361 | 7.8 | LOS A | 2.5 | 65.4 | 0.76 | 0.67 | 0.76 | 26.3 |
| 12 | R2 | 153 | 5.0 | 0.220 | 7.8 | LOS A | 1.3 | 33.1 | 0.71 | 0.64 | 0.71 | 29.7 |
| Appr |  | 494 | 5.0 | 0.361 | 7.8 | LOS A | 2.5 | 65.4 | 0.74 | 0.66 | 0.74 | 27.8 |
| All Ve | icles | 1782 | 6.2 | 0.715 | 12.9 | LOS B | 8.7 | 228.6 | 0.45 | 0.50 | 0.65 | 27.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
Site: 101 [I81 SB TERMINII - AM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| Vehicle Queue (\%ile) | 0 | 229 | 65 | 229 |



Colour code based on Queue Storage Ratio

| $\square[<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ | $\square 0.8-0.9]$ | $[0.9-1.0]$ |
| :---: | :---: | :---: | :---: | :---: |
| $[>1.0]$ |  |  |  |  |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\theta$ Site: 101 [I81 SB TERMINII - AM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| Delay (Control) | 10.9 | 21.6 | 7.8 | 12.9 |
| LOS | B | C | A | B |



Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## SITE LAYOUT

Site: 101 [I81 SB TERMINII - PM]
New Site
Site Category: (None)
Roundabout


## MOVEMENT SUMMARY

## Site: 101 [I81 SB TERMINII - PM]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 262 | 10.0 | 0.438 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 36.2 |
| 6 | T1 | 290 | 6.0 | 0.438 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 26.9 |
| Appr |  | 552 | 7.9 | 0.438 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 32.5 |
| North: 181 NB Off-ramp |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 411 | 6.0 | 0.755 | 20.4 | LOS C | 11.5 | 302.4 | 0.90 | 1.21 | 1.69 | 24.3 |
| 4 | T1 | 1 | 0.0 | 0.755 | 20.0 | LOS C | 11.5 | 302.4 | 0.90 | 1.21 | 1.69 | 27.5 |
| 14 | R2 | 205 | 7.0 | 0.755 | 20.4 | LOS C | 11.5 | 302.4 | 0.90 | 1.21 | 1.69 | 21.5 |
| Approach |  | 617 | 6.3 | 0.755 | 20.4 | LOS C | 11.5 | 302.4 | 0.90 | 1.21 | 1.69 | 23.4 |
| West: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 508 | 3.0 | 0.574 | 12.3 | LOS B | 6.3 | 160.8 | 0.91 | 0.96 | 1.20 | 22.7 |
| 12 | R2 | 198 | 8.0 | 0.333 | 10.8 | LOS B | 2.1 | 55.5 | 0.80 | 0.77 | 0.80 | 27.7 |
| Appr |  | 705 | 4.4 | 0.574 | 11.9 | LOS B | 6.3 | 160.8 | 0.88 | 0.91 | 1.09 | 24.5 |
| All V | icles | 1875 | 6.1 | 0.755 | 13.3 | LOS B | 11.5 | 302.4 | 0.63 | 0.74 | 0.97 | 25.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
( 7 Site: 101 [I81 SB TERMINII - PM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| Vehicle Queue (\%ile) | 0 | 302 | 161 | 302 |



Colour code based on Queue Storage Ratio

| $\square[<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ | $\square 0.8-0.9]$ | $[0.9-1.0]$ |
| :---: | :---: | :---: | :---: | :---: |
| $[>1.0]$ |  |  |  |  |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\theta$ Site: 101 [I81 SB TERMINII - PM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | East | North | West |  |
| Delay (Control) | 7.3 | 20.4 | 11.9 | 13.3 |
| LOS | A | C | B | B |




Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## SITE LAYOUT

$\theta$ Site: 101 [I81 NB TERMINII - AM]
New Site
Site Category: (None)
Roundabout


## MOVEMENT SUMMARY

## Site: 101 [I81 NB TERMINII - AM]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Turn | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: 181 NB On-ramp |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 197 | 4.0 | 0.565 | 12.5 | LOS B | 5.2 | 137.4 | 0.77 | 0.85 | 1.07 | 28.2 |
| 8 | T1 | 1 | 0.0 | 0.565 | 12.3 | LOS B | 5.2 | 137.4 | 0.77 | 0.85 | 1.07 | 30.8 |
| 18 | R2 | 267 | 9.0 | 0.565 | 12.8 | LOS B | 5.2 | 137.4 | 0.77 | 0.85 | 1.07 | 26.9 |
| Appr |  | 465 | 6.9 | 0.565 | 12.7 | LOS B | 5.2 | 137.4 | 0.77 | 0.85 | 1.07 | 27.5 |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 611 | 7.0 | 0.558 | 10.2 | LOS B | 5.3 | 140.9 | 0.73 | 0.68 | 0.87 | 27.3 |
| 16 | R2 | 464 | 5.0 | 0.499 | 10.2 | LOS B | 4.0 | 103.0 | 0.71 | 0.66 | 0.80 | 29.4 |
| Approach |  | 1075 | 6.1 | 0.558 | 10.2 | LOS B | 5.3 | 140.9 | 0.72 | 0.67 | 0.84 | 28.4 |
| West: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 228 | 5.0 | 0.423 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 36.7 |
| 2 | T1 | 320 | 5.0 | 0.423 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 34.2 |
| Appr |  | 548 | 5.0 | 0.423 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 35.5 |
| All Ve | icles | 2089 | 6.0 | 0.565 | 9.9 | LOS A | 5.3 | 140.9 | 0.54 | 0.53 | 0.67 | 29.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
$\theta$ Site: 101 [I81 NB TERMINII - AM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | South | East | West |  |
| Vehicle Queue (\%ile) | 137 | 141 | 0 | 141 |



Colour code based on Queue Storage Ratio

| $\square[<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ | $\square 0.8-0.9]$ | $[0.9-1.0]$ |
| :---: | :---: | :---: | :---: | :---: |
| $[>1.0]$ |  |  |  |  |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\theta$ Site: 101 [I81 NB TERMINII - AM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | South | East | West |  |
| Delay (Control) | 12.7 | 10.2 | 6.9 | 9.9 |
| LOS | B | B | A | A |



Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## SITE LAYOUT

$\theta$ Site: 101 [I81 NB TERMINII - PM]
New Site
Site Category: (None)
Roundabout


## MOVEMENT SUMMARY

## Site: 101 [I81 NB TERMINII - PM]

New Site
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: 181 NB On-ramp |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 123 | 6.0 | 0.637 | 18.6 | LOS B | 6.5 | 168.5 | 0.93 | 1.12 | 1.46 | 25.8 |
| 8 | T1 | 1 | 0.0 | 0.637 | 18.1 | LOS B | 6.5 | 168.5 | 0.93 | 1.12 | 1.46 | 28.8 |
| 18 | R2 | 274 | 4.0 | 0.637 | 18.5 | LOS B | 6.5 | 168.5 | 0.93 | 1.12 | 1.46 | 25.0 |
| Appr |  | 398 | 4.6 | 0.637 | 18.5 | LOS B | 6.5 | 168.5 | 0.93 | 1.12 | 1.46 | 25.3 |
| East: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 427 | 7.0 | 0.359 | 6.5 | LOS A | 2.3 | 61.8 | 0.55 | 0.41 | 0.55 | 30.2 |
| 16 | R2 | 310 | 4.0 | 0.301 | 6.5 | LOS A | 1.8 | 46.4 | 0.54 | 0.41 | 0.54 | 31.5 |
| Approach |  | 737 | 5.7 | 0.359 | 6.5 | LOS A | 2.3 | 61.8 | 0.55 | 0.41 | 0.55 | 30.9 |
| West: Weyers Cave |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 197 | 1.0 | 0.705 | 12.5 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 38.0 |
| 2 | T1 | 717 | 6.0 | 0.705 | 12.7 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 35.6 |
| Appr |  | 914 | 4.9 | 0.705 | 12.6 | LOS B | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 36.3 |
| All V | icles | 2048 | 5.2 | 0.705 | 11.6 | LOS B | 6.5 | 168.5 | 0.38 | 0.36 | 0.48 | 31.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## QUEUE DISTANCE (\%ILE)

Largest 95\% Back of Queue Distance for any lane used by vehicle movement (feet)
(7) Site: 101 [I81 NB TERMINII - PM]

New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | South | East | West |  |
| Vehicle Queue (\%ile) | 168 | 62 | 0 | 168 |



Colour code based on Queue Storage Ratio

| $\square[<0.6]$ | $[0.6-0.7]$ | $[0.7-0.8]$ | $\square 0.8-0.9]$ | $[0.9-1.0]$ |
| :---: | :---: | :---: | :---: | :---: |
| $[>1.0]$ |  |  |  |  |

## DELAY (CONTROL)

Average control delay per vehicle, or average pedestrian delay (seconds)
$\theta$ Site: 101 [I81 NB TERMINII - PM]
New Site
Site Category: (None)
Roundabout

## All Movement Classes

|  | Approaches |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: |
|  | South | East | West |  |
| Delay (Control) | 18.5 | 6.5 | 12.6 | 11.6 |
| LOS | B | A | B | B |



Colour code based on Level of Service
LOS A LOS B LOS C LOS D LOS E LOS F

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).
Roundabout Level of Service Method: Same as Signalised Intersections
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
6. Appendix F: VJUST Results


*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Notes |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |  |
| Information |  |  |  |  |  |  |
| Congestion | The maximum $\mathrm{v} / \mathrm{c}$ ratio represents the worst $\mathrm{v} / \mathrm{c}$ of all zones that make up an intersection. |  |  |  |  |  |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is qualitatively defined as better ( + ), similar (blank cell), or worse ( $(-)$ than a conventional intersection or traditional diamond interchange. |  |  |  |  |  |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts $)+$ Merging Conflicts + Diverging Conflicts |  |  |  |  |  |



*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Notes |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |  |
| Information |  |  |  |  |  |  |
| Congestion | The maximum $\mathrm{v} / \mathrm{c}$ ratio represents the worst $\mathrm{v} / \mathrm{c}$ of all zones that make up an intersection. |  |  |  |  |  |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is qualitatively defined as better ( + ), similar (blank cell), or worse ( $(-)$ than a conventional intersection or traditional diamond interchange. |  |  |  |  |  |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts $)+$ Merging Conflicts + Diverging Conflicts |  |  |  |  |  |

## VDOT Junction Screening Tool

## Results Worksheet

|  | General Information |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Project Title: | Route 256 at I-81 (Exit 235) - AM Peak |  |  |  |
|  | EW Facility: | Route 256 (Weyers Cave Road) |  |  |  |
|  | NS Facility: | 1-81 (Exit 235) |  |  |  |
| VDOT Junction Screening Tool | Date: | July 2, 2021 |  |  |  |
|  | Volumes (veh/hr) | U-Turn / Left | Through | Right |  |
|  | Eastbound | 203 | 97 | 135 |  |
|  | Westbound | 364 | 180 | 413 |  |
|  | Northbound | 175 | 0 | 238 |  |
|  | Southbound | 188 | 0 | 225 |  |
|  | General Instructions: All intersection and interchange configurations have a default assumption of one exclusive lane per movement. No results shall be interpreted until the user has verified the lane configurations on each worksheet. |  |  |  |  |

*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |
| Traditional Diamond | - | 0.69 |  | 28 | Turn lanes for all applicable movements. |
| Diverging Diamond | - | 0.55 | - | 20 | Turn lanes for all applicable movements. |
| Double Roundabout | - | 0.69 | + | 16 | lle-lane roundabout; NB Ramp features WBR Slip-L |
| Single Point | - | 0.51 | - | 32 | Turn lanes for all applicable movements. |

## Information

| Information |  |
| :---: | :--- |
| Congestion | The maximum v/c ratio represents the worst v/c of all zones that make up an intersection. |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is <br> qualitatively defined as better $(+)$, similar (blank cell), or worse $(-)$ than a conventional intersection or traditional diamond <br> interchange. |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts) + Merging Conflicts + Diverging Conflicts |

## VDOT Junction Screening Tool

## Results Worksheet

|  | General Information |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Project Title: | Route 256 at I-81 (Exit 235) - PM Peak |  |  |  |
|  | EW Facility: | Route 256 (Weyers Cave Road) |  |  |  |
|  | NS Facility: | 1-81 (Exit 235) |  |  |  |
| VDOT Junction Screening Tool | Date: | July 2, 2021 |  |  |  |
|  | Volumes (veh/hr) | U-Turn / Left | Through | Right |  |
|  | Eastbound | 183 | 289 | 182 |  |
|  | Westbound | 241 | 156 | 288 |  |
|  | Northbound | 114 | 0 | 255 |  |
|  | Southbound | 378 | 0 | 189 |  |
|  | General Instructions: All intersection and interchange configurations have a default assumption of one exclusive lane per movement. No results shall be interpreted until the user has verified the lane configurations on each worksheet. |  |  |  |  |

*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |
| Traditional Diamond | - | 0.75 |  | 28 | Turn lanes for all applicable movements. |
| Diverging Diamond | - | 0.71 | - | 20 | Turn lanes for all applicable movements. |
| Double Roundabout | - | 0.65 | + | 16 | lle-lane roundabout; NB Ramp features WBR Slip-L |
| Single Point | - | 0.64 | - | 32 | Turn lanes for all applicable movements. |

## Information

| Information |  |
| :---: | :--- |
| Congestion | The maximum v/c ratio represents the worst v/c of all zones that make up an intersection. |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is <br> qualitatively defined as better $(+)$, similar (blank cell), or worse $(-)$ than a conventional intersection or traditional diamond <br> interchange. |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts) + Merging Conflicts + Diverging Conflicts |


| VDOT Junction Screening Tool |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Results Worksheet |  |  |  |  |  |
|  | General Information |  |  |  |  |
|  | Project Title: | Route 256 at Triangle Drive - AM Peak |  |  |  |
|  | EW Facility: | Route 256 (Weyers Cave Road) |  |  |  |
|  | NS Facility: | Triangle Drive |  |  |  |
| VDOT Junction Screening Tool | Date: | July 1, 2021 |  |  |  |
|  | Volumes (veh/hr) | U-Turn / Left | Through | Right |  |
|  | Eastbound | 7 | 456 | 60 |  |
|  | Westbound | 28 | 905 | 10 |  |
|  | Northbound | 50 | 0 | 10 |  |
|  | Southbound | 2 | 0 | 2 |  |
|  | General Instructions: All intersection and interchange configurations have a default assumption of one exclusive lane per movement. No results shall be interpreted until the user has verified the lane configurations on each worksheet. |  |  |  |  |


*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Notes |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |  |
| Information |  |  |  |  |  |  |
| Congestion | The maximum $\mathrm{v} / \mathrm{c}$ ratio represents the worst $\mathrm{v} / \mathrm{c}$ of all zones that make up an intersection. |  |  |  |  |  |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is qualitatively defined as better ( + ), similar (blank cell), or worse ( $(-)$ than a conventional intersection or traditional diamond interchange. |  |  |  |  |  |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts $)+$ Merging Conflicts + Diverging Conflicts |  |  |  |  |  |


| VDOT Junction Screening Tool |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Results Worksheet |  |  |  |  |  |
|  | General Information |  |  |  |  |
|  | Project Title: | Route 256 at Triangle Drive - PM Peak |  |  |  |
|  | EW Facility: | Route 256 (Weyers Cave Road) |  |  |  |
|  | NS Facility: | Triangle Drive |  |  |  |
| VDOT Junction Screening Tool | Date: | July 1, 2021 |  |  |  |
|  | Volumes (veh/hr) | U-Turn / Left | Through | Right |  |
|  | Eastbound | 2 | 865 | 55 |  |
|  | Westbound | 21 | 588 | 3 |  |
|  | Northbound | 90 | 0 | 28 |  |
|  | Southbound | 10 | 0 | 7 |  |
|  | General Instructions: All intersection and interchange configurations have a default assumption of one exclusive lane per movement. No results shall be interpreted until the user has verified the lane configurations on each worksheet. |  |  |  |  |


*The continuous green-T is the only three-legged innovative intersection in this tool. To compare the continuous green-T to other innovative intersections, conflicts corresponding with the fourth leg must be removed. This has been done for the conventional intersection. Conflict point diagrams for three-legged and four-legged conventional intersections have been provided on the conventional intersection worksheet for reference.

| Interchange Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Notes |
| Type | Dir | $\begin{aligned} & \text { Maximum } \\ & \text { V/C } \end{aligned}$ | Accommodation Compared to Traditional Diamond | Weighted Total Conflict Points |  |  |
| Information |  |  |  |  |  |  |
| Congestion | The maximum $\mathrm{v} / \mathrm{c}$ ratio represents the worst $\mathrm{v} / \mathrm{c}$ of all zones that make up an intersection. |  |  |  |  |  |
| Pedestrian | Compares the potential of each design to accommodate pedestrians based on safety, wayfinding, and delay. Potential is qualitatively defined as better ( + ), similar (blank cell), or worse ( $(-)$ than a conventional intersection or traditional diamond interchange. |  |  |  |  |  |
| Safety | Weighted Total $=(2 \times$ Crossing Conflicts $)+$ Merging Conflicts + Diverging Conflicts |  |  |  |  |  |

